

ASHRAE Standard 140-2011

Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Tests

Results for Autodesk Green Building Studio 10/26/2013

vs.

Informative Annex B8, Section B8.1 Example Results

Prepared By
Autodesk

Results Developed
26-Oct-2013

ASHRAE Standard 140-2011
Computer Programs, Program Authors, and Producers of Example Results for
Section 5.2 - Building Thermal Envelope and Fabric Load Tests

The programs used to generate the example results are described in Table B11-1. Under the computer program column, the first entry in each cell is the proper program name and version number. The entries in parentheses are the abbreviations for the programs generally used in the tables and charts which follow.

The second column ("Authoring Organization") indicates the national research facility, university, or industry organization with expertise in building science that wrote the simulation software.

The third column ("Implemented By") indicates the national research facility, university, or industry organization with expertise in building science that performed the simulations. The majority of organizations that performed simulations either ran software written by their organization or otherwise ran other building energy simulation software in addition to that written by their organization.

See Standard 140, Annex B11 for further details.

TABLE B11-1
Computer Programs, Program Authors, and Producers of Example Results

| Computer Program (Abbrev.) | Authoring Organization | Example Results Produced by |
|--|--|--|
| BLAST-3.0 level 193 v.1 (BLAST-US/IT) | CERL, ^a United States (U.S.) | NREL, ^b U.S. Politecnico Torino, Italy |
| DOE-2.1D 14 (DOE21D) | LANL/LBNL, ^c U.S. | NREL, U.S. |
| ESP-RV8 (ESP-DMU) | Strathclyde University, United Kingdom (U.K.) | De Montfort University, U.K. |
| SERIRES/SUNCODE 5.7 (SRES/SUN) | NREL/Ecotope, U.S. | NREL, U.S. |
| SERIRES 1.2 (SRES-BRE) | NREL/BRE, ^d U.S./U.K. | BRE, U.K. |
| S3PAS | University of Sevilla, Spain | University of Sevilla, Spain |
| TASE | Tampere University, Finland | Tampere University, Finland |
| TRNSYS 13.1 (TSYS-BEL/BRE) | University of Wisconsin, U.S. | BRE, U.K. Vrije Universiteit (VUB) Brussels, Belgium |

^aCERL-U.S. Army Construction Engineering Research Laboratories

^bNREL-National Renewable Energy Laboratory

^cLANL/LBNL-Los Alamos National Laboratory/Lawrence Berkeley National Laboratory

^dBRE-Building Research Establishment

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Note: The statistics in the tables below are based on the Standard 140 informative example results.
 These statistics do not have any substantial importance and are not to be interpreted as acceptance criteria.

Table B8-1. Annual Heating Loads (MWh)

| Simulation Model: Organization or Country: Case | ESP DMU | BLAST US-IT | DOE21D NREL | SRES-SUN NREL | SRES* BRE | S3PAS SPAIN | TSYS BEL-BRE | TASE FINLAND | Statistics for Example Results | | | | GBS 10/26/2013 Autodesk | GBS v3.4 Autodesk |
|---|------------|----------------|----------------|------------------|--------------|----------------|-----------------|-----------------|--------------------------------|--------|--------|--------------------------|----------------------------|----------------------|
| | | | | | | | | | Min | Max | Mean | (Max-Min)/ Mean** (%) | | |
| 600 Base Case, South Windows | 4.296 | 4.773 | 5.709 | 5.226 | 5.596 | 4.882 | 4.872 | 5.362 | 4.296 | 5.709 | 5.090 | 27.8% | 4.517 | 451.7% |
| 610 S. Windows + Overhang | 4.355 | 4.806 | 5.786 | 5.280 | 5.620 | 4.971 | 4.970 | 5.383 | 4.355 | 5.786 | 5.146 | 27.8% | 4.593 | 459.3% |
| 620 East & West Windows | 4.613 | 5.049 | 5.944 | 5.554 | 5.734 | 5.564 | 5.073 | 5.728 | 4.613 | 5.944 | 5.407 | 24.6% | 5.504 | 5.504 |
| 630 E&W Windows + Overhang & Fins | 5.050 | 5.359 | 6.469 | 5.883 | 6.001 | 6.095 | 5.624 | 5.050 | 5.050 | 6.469 | 5.783 | 24.5% | 5.335 | 5.335 |
| 640 Case 600 with Htg Temp. Setback | 2.751 | 2.888 | 3.543 | 3.255 | 3.803 | 3.065 | 3.043 | 3.309 | 2.751 | 3.803 | 3.207 | 32.8% | 2.781 | 2.781 |
| 650 Case 600 with Night Ventilation | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | --- | --- | 0.000 |
| 900 South Windows | 1.170 | 1.610 | 1.872 | 1.897 | 1.988 | 1.730 | 1.655 | 2.041 | 1.170 | 2.041 | 1.745 | 49.9% | 1.648 | 1.648 |
| 910 S. Windows + Overhang | 1.575 | 1.862 | 2.254 | 2.174 | 2.282 | 2.063 | 2.097 | 2.220 | 1.575 | 2.282 | 2.066 | 34.2% | 1.526 | 1.526 |
| 920 East & West Windows | 3.313 | 3.752 | 4.255 | 4.093 | 4.058 | 4.235 | 3.776 | 4.300 | 3.313 | 4.300 | 3.973 | 24.8% | 3.884 | 3.884 |
| 930 E&W Windows + Overhang & Fins | 4.143 | 4.347 | 5.335 | 4.755 | 4.728 | 5.168 | 4.740 | 4.740 | 4.143 | 5.335 | 4.745 | 25.1% | 4.303 | 4.303 |
| 940 Case 900 with Htg Temp. Setback | 0.793 | 1.021 | 1.239 | 1.231 | 1.411 | 1.179 | 1.080 | 1.323 | 0.793 | 1.411 | 1.160 | 53.3% | 1.136 | 1.136 |
| 950 Case 900 with Night Ventilation | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | --- | --- | 0.000 |
| 960 Sunspace | 2.311 | 2.664 | 2.928 | 2.884 | 2.851 | 2.943 | 3.373 | 2.816 | 2.311 | 3.373 | 2.846 | 37.3% | 2.584 | 2.584 |
| 195 Solid Conduction | 4.167 | | | | | | | | 4.167 | 4.167 | 4.167 | 0.0% | 4.632 | 4.632 |
| 200 Surface Convection (Int & Ext IR="off") | 5.252 | | | | | | | | 5.252 | 5.252 | 5.252 | 0.0% | | |
| 210 Infrared Radiation (Int IR="off", Ext IR="on") | 6.456 | 6.559 | | | | | 6.554 | 6.967 | 6.456 | 6.967 | 6.634 | 7.7% | | |
| 215 Infrared Radiation (Int IR="on", Ext IR="off") | 5.547 | | | | | | | | 5.547 | 5.547 | 5.547 | 0.0% | 7.268 | 726.8% |
| 220 In-Depth Base Case | 6.944 | 7.215 | 8.787 | 8.102 | 8.127 | 7.422 | 7.297 | 7.437 | 6.944 | 8.787 | 7.666 | 24.0% | 8.365 | 836.5% |
| 230 Infiltration | 10.376 | 10.740 | 12.243 | 11.633 | 11.649 | 11.037 | 10.840 | 10.964 | 10.376 | 12.243 | 11.185 | 16.7% | 11 | 1092.3% |
| 240 Internal Gains | 5.649 | 6.009 | 7.448 | 6.769 | 6.786 | 6.194 | 6.076 | 6.234 | 5.649 | 7.448 | 6.396 | 28.1% | 7 | 7.041 |
| 250 Exterior Shortwave Absorptance | 4.751 | 5.739 | 7.024 | 6.608 | 6.653 | 5.974 | 5.764 | 5.738 | 4.751 | 7.024 | 6.031 | 37.7% | 6 | 5.913 |
| 270 South Solar Windows | 4.510 | 4.930 | | 5.341 | 5.920 | | 5.047 | 5.489 | 4.510 | 5.920 | 5.206 | 27.1% | 5 | 5.006 |
| 280 Cavity Albedo | 4.675 | 5.125 | | 5.937 | 6.148 | | 5.279 | 5.841 | 4.675 | 6.148 | 5.501 | 26.8% | 5 | 5.281 |
| 290 South Shading | 4.577 | 4.959 | | 5.406 | 5.942 | | 5.132 | 5.509 | 4.577 | 5.942 | 5.254 | 26.0% | 5.646 | 5.646 |
| 300 East/West Window | 4.761 | 5.077 | | 5.587 | 5.964 | | 5.124 | 5.786 | 4.761 | 5.964 | 5.383 | 22.3% | 5.826 | 5.826 |
| 310 East/West Shading | 5.221 | 5.327 | | 5.850 | 6.165 | | 5.610 | 5.610 | 5.221 | 6.165 | 5.635 | 16.8% | 5.787 | 5.787 |
| 320 Thermostat | 3.859 | 4.209 | | 4.627 | 5.141 | | 4.348 | 4.840 | 3.859 | 5.141 | 4.504 | 28.5% | 4.230 | 4.230 |
| 395 Low Mass Solid Conduction | 4.984 | 4.799 | 5.835 | 5.199 | 5.201 | 4.967 | 4.855 | 4.839 | 4.799 | 5.835 | 5.085 | 20.4% | 5.783 | 5.783 |
| 400 Low Mass Opaque Windows | 6.900 | 7.075 | 8.770 | 7.966 | 7.973 | 7.287 | 7.166 | 7.326 | 6.900 | 8.770 | 7.558 | 24.7% | 8.334 | 8.334 |
| 410 Low Mass Infiltration | 8.596 | 8.873 | 10.506 | 9.726 | 9.734 | 9.019 | 8.936 | 9.085 | 8.596 | 10.506 | 9.309 | 20.5% | 9 | 9.268 |
| 420 Low Mass Internal Gains | 7.298 | 7.610 | 9.151 | 8.365 | 8.373 | 7.774 | 7.697 | 7.863 | 7.298 | 9.151 | 8.016 | 23.1% | 8 | 7.923 |
| 430 Low Mass Ext. Shortwave Absorptance | 5.429 | 6.488 | 7.827 | 7.178 | 7.186 | 6.662 | 6.500 | 6.510 | 5.429 | 7.827 | 6.723 | 35.7% | 6.385 | 638.5% |
| 440 Low Mass Cavity Albedo | 4.449 | 4.987 | | 5.652 | 5.811 | | 5.098 | 5.642 | 4.449 | 5.811 | 5.273 | 25.8% | 4.801 | 480.1% |
| 800 High Mass Opaque Windows | 4.868 | 5.953 | 7.228 | 6.611 | 6.600 | 6.161 | 5.940 | 5.861 | 4.868 | 7.228 | 6.153 | 38.4% | 6.325 | 632.5% |
| 810 High Mass Cavity Albedo | 1.839 | 2.446 | | 3.004 | 2.828 | | 2.567 | 2.962 | 1.839 | 3.004 | 2.608 | 44.7% | 2.130 | 213.0% |

* SRES-BRE (SERIRES 1.2) simulations for cases with interior solar absorptance = 0.9 have an input error that likely affects annual heating and cooling loads by <0.2 MWh/y (2-3%); see Section B7.2.

** ABS[(Max-Min) / (Mean of Example Simulation Results)]

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Table B8-2. Annual Sensible Cooling Loads (MWh)

| Simulation Model: Organization or Country: Case | ESP DMU | BLAST US-IT | DOE21D NREL | SRES-SUN NREL | SRES* BRE | S3PAS SPAIN | TSYS BEL-BRE | TASE FINLAND | Statistics for Example Results | | | | GBS 10/26/2013 Autodesk | GBS v3.4 Autodesk |
|---|------------|----------------|----------------|------------------|--------------|----------------|-----------------|-----------------|--------------------------------|--------|-------|--------------------------|----------------------------|----------------------|
| | | | | | | | | | Min | Max | Mean | (Max-Min)/ Mean** (%) | | |
| 600 Base Case, South Windows | 6.137 | 6.433 | 7.079 | 7.278 | 7.964 | 6.492 | 6.492 | 6.778 | 6.137 | 7.964 | 6.832 | 26.7% | 7.697 | 7.697 |
| 610 S. Windows + Overhang | 3.915 | 4.851 | 4.852 | 5.448 | 5.778 | 4.764 | 4.601 | 5.506 | 3.915 | 5.778 | 4.964 | 37.5% | 5.650 | 5.650 |
| 620 East & West Windows | 3.417 | 4.092 | 4.334 | 4.633 | 5.004 | 4.011 | 3.901 | 4.351 | 3.417 | 5.004 | 4.218 | 37.6% | 4.915 | 4.915 |
| 630 E&W Windows + Overhang & Fins | 2.129 | 3.108 | 2.489 | 3.493 | 3.701 | 2.489 | 2.416 | 2.489 | 2.129 | 3.701 | 2.832 | 55.5% | 2.942 | 2.942 |
| 640 Case 600 with Htg Temp. Setback | 5.952 | 6.183 | 6.759 | 7.026 | 7.811 | 6.247 | 6.246 | 6.508 | 5.952 | 7.811 | 6.592 | 28.2% | 7.351 | 7.351 |
| 650 Case 600 with Night Ventilation | 4.816 | 5.140 | 5.795 | 5.894 | 6.545 | 5.088 | 5.119 | 5.456 | 4.816 | 6.545 | 5.482 | 31.5% | 5.726 | 5.726 |
| 900 South Windows | 2.132 | 2.600 | 2.455 | 3.165 | 3.415 | 2.572 | 2.485 | 2.599 | 2.132 | 3.415 | 2.678 | 47.9% | 3.237 | 3.237 |
| 910 S. Windows + Overhang | 0.821 | 1.533 | 0.976 | 1.872 | 1.854 | 1.428 | 1.326 | 1.767 | 0.821 | 1.872 | 1.447 | 72.6% | 1.764 | 1.764 |
| 920 East & West Windows | 1.840 | 2.616 | 2.440 | 2.943 | 3.092 | 2.457 | 2.418 | 2.613 | 1.840 | 3.092 | 2.552 | 49.1% | 3.093 | 3.093 |
| 930 E&W Windows + Overhang & Fins | 1.039 | 1.934 | 1.266 | 2.173 | 2.238 | 1.439 | 1.416 | 1.439 | 1.039 | 2.238 | 1.644 | 73.0% | 1.781 | 1.781 |
| 940 Case 900 with Htg. Temp. Setback | 2.079 | 2.536 | 2.340 | 3.036 | 3.241 | 2.489 | 2.383 | 2.516 | 2.079 | 3.241 | 2.578 | 45.1% | 3.108 | 3.108 |
| 950 Case 900 with Night Ventilation | 0.387 | 0.526 | 0.538 | 0.921 | 0.589 | 0.551 | 0.561 | 0.771 | 0.387 | 0.921 | 0.605 | 88.2% | 0.746 | 0.746 |
| 960 Sunspace | 0.488 | 0.666 | 0.428 | 0.803 | 0.718 | 0.643 | 0.411 | 0.786 | 0.411 | 0.803 | 0.618 | 63.4% | 0.752 | 0.752 |
| 195 Solid Conduction | 0.414 | | | | | | | | 0.414 | 0.414 | 0.414 | 0.0% | 0.621 | 0.621 |
| 200 Surface Convection (Int & Ext IR="off") | 0.570 | | | | | | | | 0.570 | 0.570 | 0.570 | 0.0% | | |
| 210 Infrared Radiation (Int IR="off", Ext IR="on") | 0.162 | 0.613 | | | | | 0.668 | 0.641 | 0.162 | 0.668 | 0.521 | 97.1% | | |
| 215 Infrared Radiation (Int IR="on", Ext IR="off") | 0.639 | | | | | | | | 0.639 | 0.639 | 0.639 | 0.0% | 0.644 | 0.644 |
| 220 In-Depth Base Case | 0.186 | 0.701 | 0.399 | 0.827 | 0.835 | 0.734 | 0.737 | 0.683 | 0.186 | 0.835 | 0.638 | 101.8% | 0.380 | 0.380 |
| 230 Infiltration | 0.454 | 0.976 | 0.692 | 1.131 | 1.139 | 1.020 | 1.040 | 0.985 | 0.454 | 1.139 | 0.930 | 73.7% | 0.613 | 0.613 |
| 240 Internal Gains | 0.415 | 1.072 | 0.660 | 1.239 | 1.246 | 1.108 | 1.114 | 1.045 | 0.415 | 1.246 | 0.987 | 84.2% | 0.636 | 0.636 |
| 250 Exterior Shortwave Absorptance | 3.213 | 2.545 | 2.177 | 2.924 | 2.931 | 2.486 | 2.684 | 3.380 | 2.177 | 3.380 | 2.793 | 43.1% | 3.342 | 3.342 |
| 270 South Solar Windows | 7.528 | 8.670 | | 9.828 | 10.350 | | 8.764 | 8.714 | 7.528 | 10.350 | 8.976 | 31.4% | 9.287 | 9.287 |
| 280 Cavity Albedo | 4.873 | 5.895 | | 6.511 | 7.114 | | 5.761 | 6.257 | 4.873 | 7.114 | 6.069 | 36.9% | 6.130 | 6.130 |
| 290 South Shading | 5.204 | 7.011 | | 7.871 | 8.089 | | 6.699 | 7.431 | 5.204 | 8.089 | 7.051 | 40.9% | 6.771 | 6.771 |
| 300 East/West Window | 4.302 | 5.836 | | 6.665 | 7.100 | | 5.721 | 5.781 | 4.302 | 7.100 | 5.901 | 47.4% | 6.020 | 6.020 |
| 310 East/West Shading | 2.732 | 4.570 | | 5.245 | 5.471 | | 3.727 | 3.727 | 2.732 | 5.471 | 4.349 | 63.0% | 3.639 | 3.639 |
| 320 Thermostat | 5.061 | 5.906 | | 6.725 | 7.304 | | 5.956 | 5.663 | 5.061 | 7.304 | 6.103 | 36.8% | 5.986 | 5.986 |
| 395 Low Mass Solid Conduction | 0.000 | 0.011 | 0.000 | 0.016 | 0.014 | 0.010 | 0.010 | 0.011 | 0.000 | 0.016 | 0.009 | 177.1% | 0.000 | 0.000 |
| 400 Low Mass Opaque Windows | 0.000 | 0.040 | 0.002 | 0.061 | 0.058 | 0.042 | 0.045 | 0.044 | 0.000 | 0.061 | 0.036 | 167.3% | 0.001 | 0.001 |
| 410 Low Mass Infiltration | 0.000 | 0.059 | 0.010 | 0.084 | 0.084 | 0.063 | 0.067 | 0.065 | 0.000 | 0.084 | 0.054 | 155.5% | 0.004 | 0.004 |
| 420 Low Mass Internal Gains | 0.011 | 0.147 | 0.051 | 0.189 | 0.188 | 0.154 | 0.158 | 0.143 | 0.011 | 0.189 | 0.130 | 136.9% | 0.034 | 0.034 |
| 430 Low Mass Ext. Shortwave Absorptance | 0.542 | 0.617 | 0.422 | 0.704 | 0.684 | 0.563 | 0.617 | 0.875 | 0.422 | 0.875 | 0.628 | 72.1% | 0.943 | 0.943 |
| 440 Low Mass Cavity Albedo | 3.967 | 4.172 | | 4.674 | 5.204 | | 3.975 | 4.684 | 3.967 | 5.204 | 4.446 | 27.8% | 4.729 | 4.729 |
| 800 High Mass Opaque Windows | 0.113 | 0.224 | 0.055 | 0.272 | 0.222 | 0.195 | 0.207 | 0.325 | 0.055 | 0.325 | 0.202 | 133.9% | 0.091 | 0.091 |
| 810 High Mass Cavity Albedo | 1.052 | 1.405 | | 1.711 | 1.708 | | 1.191 | 1.624 | 1.052 | 1.711 | 1.449 | 45.5% | 1.656 | 1.656 |

* SRES-BRE (SERIRES 1.2) simulations for cases with interior solar absorptance = 0.9 have an input error that likely affects annual heating and cooling loads by <0.2 MWh/y (2-3%); see Section B7.2.

Affected results for Cases 270 and 290 through 320 are indicated by italics

** ABS[(Max-Min) / (Mean of Example Simulation Results)]

**ASHRAE Standard 140-2011 Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Tests
Autodesk Green Building Studio 10/26/2013 vs. Annex B8, Section B8.1 Example Results**

By Autodesk, 26-Oct-2013
Note: The statistics in the tables below are based on the Standard 140 informative example results.
These statistics do not have any substantial importance and are not to be interpreted as acceptance criteria.

Table B8-5. Free-Float Temperature Output

| MAXIMUM ANNUAL HOURLY INTEGRATED ZONE TEMPERATURE | | | | | | | | | | | | | | Example Result Statistics | | | | GBS 10/26/2013 Autodesk | | | GBS v3.4 Autodesk | | | | | | | | | | |
|---|-------------------|--------|---------|--------|-------------|----|-------------|--------|---------------|--------|-----------|----|-------------|---------------------------|--------------|--------|--------------|-------------------------|--------|--------|-------------------|------------|--------|------|-------|--------|--------|----|------|--------|----|
| Case | Simulation Model: | | ESP DMU | | BLAST US-IT | | DOE21D NREL | | SRES-SUN NREL | | SRES BRE* | | S3PAS SPAIN | | TSYS BEL-BRE | | TASE FINLAND | | Min | Max | Mean | (Max-Min) | T (°C) | Date | Hr | T (°C) | Date | Hr | | | |
| | T (°C) | Date | Hr | T (°C) | Date | Hr | T (°C) | Date | Hr | T (°C) | Date | Hr | T (°C) | Date | Hr | T (°C) | Date | Hr | T (°C) | T (°C) | T (°C) | Mean** (%) | T (°C) | Date | Hr | T (°C) | Date | Hr | | | |
| 600FF - Low Mass with S. Windows | 64.9 | 17-Oct | 15 | 65.1 | 16-Oct | 15 | 69.5 | 17-Oct | 15 | 68.6 | 16-Oct | 15 | 64.9 | 16-Oct | 16 | 65.3 | 17-Oct | 16 | 65.3 | 15-Oct | 16 | 64.9 | 69.5 | 66.2 | 6.9% | 67.1 | 17-Oct | 16 | 67.1 | 17-Oct | 16 |
| 900FF - High Mass with S. Windows | 41.8 | 17-Oct | 15 | 43.4 | 02-Sep | 16 | 42.7 | 02-Sep | 15 | 44.8 | 02-Sep | 15 | 43.0 | 02-Sep | 15 | 42.5 | 17-Oct | 15 | 43.2 | 15-Sep | 15 | 41.8 | 44.8 | 43.1 | 6.9% | 44.8 | 17-Oct | 16 | 44.8 | #### | 15 |
| 650FF Case 600FF with Night Ventilation | 63.2 | 17-Oct | 15 | 63.5 | 16-Oct | 15 | 68.2 | 17-Oct | 15 | 67.0 | 16-Oct | 15 | 63.3 | 16-Oct | 16 | 63.7 | 17-Oct | 16 | 63.8 | 16-Oct | 16 | 63.2 | 68.2 | 64.7 | 7.7% | 64.1 | 17-Oct | 16 | 64.1 | 17-Oct | 16 |
| 950FF Case 900FF with Night Ventilation | 35.5 | 02-Sep | 16 | 36.2 | 02-Sep | 16 | 35.9 | 02-Sep | 16 | 38.5 | 02-Sep | 15 | 36.1 | 02-Sep | 16 | 35.7 | 02-Sep | 15 | 37.6 | 15-Sep | 16 | 35.5 | 38.5 | 36.5 | 8.1% | 37.1 | 17-Oct | 16 | 37.1 | #### | 16 |
| 960 Sunspace | 48.9 | 17-Oct | 15 | 48.9 | 06-Oct | 15 | 49.0 | 17-Oct | 15 | 51.0 | 17-Oct | 15 | 50.2 | 17-Oct | 15 | 55.3 | 17-Oct | 15 | 48.9 | 15-Oct | 15 | 48.9 | 55.3 | 50.3 | 12.8% | 50.4 | 17-Oct | 15 | 50.4 | 17-Oct | 15 |

| MINIMUM ANNUAL HOURLY INTEGRATED ZONE TEMPERATURE | | | | | | | | | | | | | | Example Result Statistics | | | | GBS 10/26/2013 Autodesk | | | GBS v3.4 Autodesk | | | | | | | | | | |
|---|-------------------|--------|---------|--------|-------------|----|-------------|--------|---------------|--------|-----------|----|-------------|---------------------------|--------------|--------|--------------|-------------------------|--------|--------|-------------------|------------|--------|-------|--------|--------|--------|----|--------|--------|----|
| Case | Simulation Model: | | ESP DMU | | BLAST US-IT | | DOE21D NREL | | SRES-SUN NREL | | SRES BRE* | | S3PAS SPAIN | | TSYS BEL-BRE | | TASE FINLAND | | Min | Max | Mean | (Max-Min) | T (°C) | Date | Hr | T (°C) | Date | Hr | T (°C) | Date | Hr |
| | T (°C) | Date | Hr | T (°C) | Date | Hr | T (°C) | Date | Hr | T (°C) | Date | Hr | T (°C) | Date | Hr | T (°C) | Date | Hr | T (°C) | T (°C) | T (°C) | Mean** (%) | T (°C) | Date | Hr | T (°C) | Date | Hr | T (°C) | Date | Hr |
| 600FF - Low Mass with S. Windows | -15.6 | 04-Jan | 7 | -17.1 | 04-Jan | 8 | -18.8 | 04-Jan | 8 | -19.0 | 04-Jan | 7 | -17.9 | 04-Jan | 8 | -17.9 | 04-Jan | 7 | -18.5 | 08-Jan | 9 | -18.8 | -15.6 | -17.6 | 18.3% | -16.1 | 03-Jan | 8 | -16.1 | 03-Jan | 8 |
| 900FF - High Mass with S. Windows | -1.6 | 04-Jan | 8 | -3.2 | 04-Jan | 8 | -4.3 | 04-Jan | 8 | -4.5 | 04-Jan | 8 | -4.0 | 04-Jan | 8 | -6.4 | 04-Jan | 8 | -5.6 | 08-Jan | 9 | -6.4 | -1.6 | -4.2 | 111.9% | -1.9 | 04-Jan | 8 | -1.9 | 04-Jan | 8 |
| 650FF Case 600FF with Night Ventilation | -22.6 | 04-Jan | 6 | -23.0 | 04-Jan | 7 | -21.6 | 04-Jan | 2 | -23.0 | 04-Jan | 2 | -22.9 | 04-Jan | 2 | -22.8 | 04-Jan | 7 | -22.9 | 02-Jan | 23 | -23.0 | -21.6 | -22.7 | 6.2% | -17.3 | 04-Jan | 8 | -17.3 | 04-Jan | 8 |
| 950FF Case 900FF with Night Ventilation | -19.5 | 04-Jan | 6 | -20.0 | 04-Jan | 7 | -18.6 | 04-Jan | 7 | -19.7 | 04-Jan | 7 | -20.2 | 04-Jan | 7 | -19.3 | 04-Jan | 8 | -20.0 | 07-Jan | 22 | -20.2 | -18.6 | -19.6 | 8.2% | -14.5 | 04-Jan | 7 | -14.5 | 04-Jan | 7 |
| 960 Sunspace | 2.7 | 06-Feb | 6 | 1.6 | 06-Feb | 7 | 3.9 | 06-Feb | 7 | 3.1 | 06-Feb | 7 | 1.4 | 06-Feb | 6 | -2.8 | 04-Jan | 8 | -0.4 | 05-Feb | 7 | -2.8 | 3.9 | 1.4 | 492.6% | 5.8 | 06-Feb | 7 | 5.8 | 06-Feb | 7 |

| AVERAGE ANNUAL HOURLY INTEGRATED ZONE TEMPERATURE | | | | | | | | | | | | | | Example Result Statistics | | | | GBS 10/26/2013 Autodesk | | | GBS v3.4 Autodesk | | | | | | | | | | |
|---|-------------------|------|---------|--------|-------------|----|-------------|------|---------------|--------|----------|----|-------------|---------------------------|--------------|--------|--------------|-------------------------|--------|--------|-------------------|------------|--------|------|----|--------|------|----|--------|------|----|
| Case | Simulation Model: | | ESP DMU | | BLAST US-IT | | DOE21D NREL | | SRES-SUN NREL | | SRES BRE | | S3PAS SPAIN | | TSYS BEL-BRE | | TASE FINLAND | | Min | Max | Mean | (Max-Min) | T (°C) | Date | Hr | T (°C) | Date | Hr | T (°C) | Date | Hr |
| | T (°C) | Date | Hr | T (°C) | Date | Hr | T (°C) | Date | Hr | T (°C) | Date | Hr | T (°C) | Date | Hr | T (°C) | Date | Hr | T (°C) | T (°C) | T (°C) | Mean** (%) | T (°C) | Date | Hr | T (°C) | Date | Hr | T (°C) | Date | Hr |
| 600FF - Low Mass with S. Windows | 25.1 | | | 25.4 | | | 24.6 | | | 25.5 | | | 25.9 | | | 24.5 | | | 24.2 | 25.9 | 25.1 | 6.8% | 27.1 | | | 27.1 | | | 27.1 | | |
| 900FF - High Mass with S. Windows | 25.5 | | | 25.9 | | | 24.7 | | | 25.5 | | | 25.7 | | | 24.5 | | | 24.5 | 25.9 | 25.2 | 5.9% | 27.1 | | | 27.1 | | | 27.1 | | |
| 650FF Case 600FF with Night Ventilation | 18.2 | | | 18.7 | | | 19.1 | | | 19.0 | | | 19.6 | | | 18.0 | | | 18.0 | 19.6 | 18.7 | 8.7% | 19.9 | | | 19.9 | | | 19.9 | | |
| 950FF Case 900FF with Night Ventilation | 14.1 | | | 14.3 | | | 14.3 | | | 15.0 | | | 14.3 | | | 14.0 | | | 14.6 | 15.0 | 14.4 | 6.7% | 15.9 | | | 15.9 | | | 15.9 | | |
| 960 Sunspace | 27.5 | | | 27.7 | | | 28.0 | | | 28.7 | | | 28.5 | | | 28.0 | | | 28.4 | 29.0 | 28.0 | 9.0% | 29.7 | | | 29.7 | | | 29.7 | | |

* SRES-BRE (SERIRES 1.2) simulations did not produce output for this variable.
** ABS (Max-Min) / (Mean of Example Simulation Results)

**ASHRAE Standard 140-2011 Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Tests
Autodesk Green Building Studio 10/26/2013 vs. Annex B8, Section B8.1 Example Results
By Autodesk , 26-Oct-2013**

Note: The statistics in the tables below are based on the Standard 140 informative example results.
These statistics do not have any substantial importance and are not to be interpreted as acceptance criteria.

Table B8-9. Low Mass In-Depth (Cases 395 thru 440) Sensitivity Tests

| ANNUAL HEATING [MWh] | | | | | | | | | | Statistics for Example Results | | | | GBS 10/26/2013 Autodesk | GBS v3.4 Autodesk |
|-------------------------------|------------|----------------|----------------|------------------|--------------|----------------|-----------------|-----------------|--------|--------------------------------|--------|-------------------------|--------|----------------------------|----------------------|
| CASES | ESP DMU | BLAST US-IT | DOE21D NREL | SRES-SUN NREL | SRES BRE | S3PAS SPAIN | TSYS BEL-BRE | TASE FINLAND | Min | Max | Mean | (Max-Min) Mean** (%) | | | |
| 400-395 Surf. Conv. & IR | 1.916 | 2.276 | 2.935 | 2.767 | 2.772 | 2.320 | 2.311 | 2.487 | 1.916 | 2.935 | 2.473 | 41.2% | 2.551 | 255.1% | |
| 410-400 Infiltration | 1.696 | 1.798 | 1.736 | 1.760 | 1.761 | 1.732 | 1.770 | 1.759 | 1.696 | 1.798 | 1.752 | 5.8% | 0.934 | 93.4% | |
| 420-410 Internal Gains | -1.298 | -1.263 | -1.355 | -1.361 | -1.361 | -1.245 | -1.239 | -1.222 | -1.361 | -1.222 | -1.293 | 10.8% | -1.345 | -1.345 | |
| 430-420 Ext Solar Abs. | -1.869 | -1.122 | -1.324 | -1.187 | -1.187 | -1.112 | -1.197 | -1.353 | -1.869 | -1.112 | -1.294 | 58.5% | -1.538 | -1.538 | |
| 600-430 South Windows | -1.133 | -1.715 | -2.118 | -1.952 | -1.590 | -1.780 | -1.628 | -1.148 | -2.118 | -1.133 | -1.633 | 60.3% | -1.868 | -1.868 | |
| 440-600 Cavity Albedo | 0.153 | 0.214 | | 0.426 | 0.215 | | 0.226 | 0.280 | 0.153 | 0.426 | 0.252 | 108.2% | 0.284 | 0.284 | |
| ANNUAL SENSIBLE COOLING [MWh] | | | | | | | | | | Statistics for Example Results | | | | GBS 10/26/2013 Autodesk | GBS v3.4 Autodesk |
| CASES | ESP DMU | BLAST US-IT | DOE21D NREL | SRES-SUN NREL | SRES BRE | S3PAS SPAIN | TSYS BEL-BRE | TASE FINLAND | Min | Max | Mean | (Max-Min) Mean** (%) | | | |
| 400-395 Surf. Conv. & IR | 0.000 | 0.029 | 0.002 | 0.045 | 0.044 | 0.032 | 0.034 | 0.033 | 0.000 | 0.045 | 0.027 | 164.1% | 0.001 | 0.001 | |
| 410-400 Infiltration | 0.000 | 0.019 | 0.008 | 0.023 | 0.026 | 0.021 | 0.022 | 0.021 | 0.000 | 0.026 | 0.018 | 148.2% | 0.003 | 0.003 | |
| 420-410 Internal Gains | 0.011 | 0.088 | 0.041 | 0.105 | 0.104 | 0.091 | 0.090 | 0.078 | 0.011 | 0.105 | 0.076 | 123.6% | 0.030 | 0.030 | |
| 430-420 Ext Solar Abs. | 0.531 | 0.470 | 0.371 | 0.515 | 0.496 | 0.409 | 0.460 | 0.732 | 0.371 | 0.732 | 0.498 | 72.5% | 0.910 | 0.910 | |
| 600-430 South Windows | 5.595 | 5.816 | 6.657 | 6.574 | 7.280 | 5.929 | 5.875 | 5.903 | 5.595 | 7.280 | 6.204 | 27.2% | 6.754 | 6.754 | |
| 440-600 Cavity Albedo | -2.170 | -2.261 | | -2.604 | -2.760 | | -2.517 | -2.094 | -2.760 | -2.094 | -2.401 | 27.7% | -2.969 | -296.9% | |
| PEAK HEATING [kW] | | | | | | | | | | Statistics for Example Results | | | | GBS 10/26/2013 Autodesk | GBS v3.4 Autodesk |
| CASES | ESP DMU | BLAST US-IT | DOE21D NREL | SRES-SUN NREL | SRES BRE* | S3PAS SPAIN | TSYS BEL-BRE | TASE FINLAND | Min | Max | Mean | (Max-Min) Mean** (%) | | | |
| 400-395 Surf. Conv. & IR | 0.805 | 1.071 | 1.148 | 1.310 | | 1.079 | 1.115 | 1.250 | 0.805 | 1.310 | 1.111 | 45.4% | 1 | 99.0% | |
| 410-400 Infiltration | 0.758 | 0.844 | 0.757 | 0.792 | | 0.885 | 0.778 | 0.794 | 0.757 | 0.885 | 0.801 | 16.0% | 0 | 0.492 | |
| 420-410 Internal Gains | -0.182 | -0.180 | -0.183 | -0.200 | | -0.183 | -0.183 | -0.188 | -0.200 | -0.180 | -0.186 | 10.8% | 0 | -0.182 | |
| 430-420 Ext Solar Abs. | -0.001 | 0.000 | 0.000 | 0.000 | | 0.000 | 0.000 | 0.011 | -0.001 | 0.011 | 0.001 | 840.0% | 0 | 0.282 | |
| 600-430 South Windows | -0.005 | -0.004 | -0.005 | -0.029 | | -0.007 | 0.000 | 0.217 | -0.029 | 0.217 | 0.024 | 1031.1% | 0 | -0.039 | |
| 440-600 Cavity Albedo | 0.002 | 0.002 | | 0.019 | | | 0.000 | 0.022 | 0.000 | 0.022 | 0.009 | 244.4% | 0.000 | 0.000 | |
| PEAK SENSIBLE COOLING [kW] | | | | | | | | | | Statistics for Example Results | | | | GBS 10/26/2013 Autodesk | GBS v3.4 Autodesk |
| CASES | ESP DMU | BLAST US-IT | DOE21D NREL | SRES-SUN NREL | SRES BRE* | S3PAS SPAIN | TSYS BEL-BRE | TASE FINLAND | Min | Max | Mean | (Max-Min) Mean** (%) | | | |
| 400-395 Surf. Conv. & IR | 0.000 | 0.219 | 0.265 | 0.272 | | 0.256 | 0.251 | 0.227 | 0.000 | 0.272 | 0.213 | 127.8% | 0.193 | 0.193 | |
| 410-400 Infiltration | 0.035 | 0.118 | 0.148 | 0.148 | | 0.112 | 0.130 | 0.138 | 0.035 | 0.148 | 0.118 | 95.4% | 0.124 | 0.124 | |
| 420-410 Internal Gains | 0.223 | 0.224 | 0.218 | 0.233 | | 0.214 | 0.195 | 0.211 | 0.195 | 0.233 | 0.217 | 17.7% | 0 | 0.297 | |
| 430-420 Ext Solar Abs. | 1.235 | 0.849 | 0.796 | 0.715 | | 0.637 | 0.861 | 1.657 | 0.637 | 1.657 | 0.964 | 105.8% | 1 | 1.442 | |
| 600-430 South Windows | 4.701 | 4.193 | 5.229 | 5.065 | | 4.711 | 4.688 | 4.234 | 4.193 | 5.229 | 4.689 | 22.1% | 4.564 | 456.4% | |
| 440-600 Cavity Albedo | -1.648 | -1.541 | | -1.774 | | | -1.800 | -1.534 | -1.800 | -1.534 | -1.659 | 16.0% | -1.804 | -180.4% | |

* SRES-BRE (SERIRES 1.2) simulations did not produce output for this variable.

** ABS[(Max-Min) / (Mean of Example Simulation Results)]

**ASHRAE Standard 140-2011 Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Tests
Autodesk Green Building Studio 10/26/2013 vs. Annex B8, Section B8.1 Example Results
By Autodesk , 26-Oct-2013**

Note: The statistics in the tables below are based on the Standard 140 informative example results.
These statistics do not have any substantial importance and are not to be interpreted as acceptance criteria.

Table B8-10. High Mass Basic and In-Depth Sensitivity Tests

| | | | | | | | | | | | | | | 10/26/2013 | GBS v3.4 |
|--------------------------------|---------|-------------|-------------|---------------|-----------|-------------|--------------|--------------|--------|--------------------------------|--------|----------------------|----------|------------|----------|
| ANNUAL HEATING [MWh] | | | | | | | | | | Statistics for Example Results | | | | 10/26/2013 | GBS v3.4 |
| CASES | ESP DMU | BLAST US-IT | DOE21D NREL | SRES-SUN NREL | SRES BRE | S3PAS SPAIN | TSYS BEL-BRE | TASE FINLAND | Min | Max | Mean | (Max-Min)/Mean** (%) | Autodesk | Autodesk | |
| 800-430 Mass, w/ Op. Win. | -0.561 | -0.535 | -0.599 | -0.567 | -0.586 | -0.501 | -0.560 | -0.649 | -0.649 | -0.501 | -0.570 | 26.0% | -0.060 | -0.060 | |
| 900-800 Himass, S. Win. | -3.698 | -4.343 | -5.356 | -4.714 | -4.612 | -4.431 | -4.285 | -3.820 | -5.356 | -3.698 | -4.407 | 37.6% | -4.677 | -4.677 | |
| 900-810 Himass, Int. Sol. Abs. | -0.669 | -0.836 | | -1.107 | -0.840 | | -0.912 | -0.921 | -1.107 | -0.669 | -0.881 | 49.7% | -0.482 | -0.482 | |
| 910-610 Mass, w/ S. Shade | -2.780 | -2.944 | -3.532 | -3.106 | -3.338 | -2.908 | -2.873 | -3.163 | -3.532 | -2.780 | -3.081 | 24.4% | -3.067 | -3.067 | |
| 920-620 Mass, w/ E&W Win. | -1.300 | -1.297 | -1.689 | -1.461 | -1.676 | -1.329 | -1.297 | -1.428 | -1.689 | -1.297 | -1.435 | 27.3% | -1.620 | -1.620 | |
| 930-630 Mass w/ E&W Shade | -0.907 | -1.012 | -1.134 | -1.128 | -1.273 | -0.927 | -0.884 | | -1.273 | -0.884 | -1.038 | 37.5% | -1.031 | -1.031 | |
| 940-640 Mass, w/ Htg. Setback | -1.958 | -1.867 | -2.304 | -2.024 | -2.392 | -1.886 | -1.963 | -1.986 | -2.392 | -1.867 | -2.048 | 25.6% | -1.645 | -1.645 | |
| ANNUAL SENSIBLE COOLING [MWh] | | | | | | | | | | Statistics for Example Results | | | | 10/26/2013 | GBS v3.4 |
| CASES | ESP DMU | BLAST US-IT | DOE21D NREL | SRES-SUN NREL | SRES BRE | S3PAS SPAIN | TSYS BEL-BRE | TASE FINLAND | Min | Max | Mean | (Max-Min)/Mean** (%) | Autodesk | Autodesk | |
| 800-430 Mass, w/ Op. Win. | -0.429 | -0.393 | -0.367 | -0.432 | -0.462 | -0.368 | -0.410 | -0.550 | -0.550 | -0.367 | -0.426 | 42.9% | -0.852 | -0.852 | |
| 900-800 Himass, S. Win. | 2.019 | 2.376 | 2.400 | 2.893 | 3.193 | 2.377 | 2.278 | 2.274 | 2.019 | 3.193 | 2.476 | 47.4% | 3.145 | 3.145 | |
| 900-810 Himass, Int. Sol. Abs. | 1.080 | 1.195 | | 1.454 | 1.707 | | 1.294 | 0.975 | 1.075 | 1.707 | 1.284 | 57.0% | 1.581 | 1.581 | |
| 910-610 Mass, w/ S. Shade | -3.094 | -3.318 | -3.876 | -3.576 | -3.924 | -3.336 | -3.275 | -3.739 | -3.924 | -3.094 | -3.517 | 23.6% | -3.886 | -3.886 | |
| 920-620 Mass, w/ E&W Win. | -1.577 | -1.476 | -1.894 | -1.690 | -1.912 | -1.554 | -1.483 | -1.738 | -1.912 | -1.476 | -1.666 | 26.2% | -1.822 | -1.822 | |
| 930-630 Mass w/ E&W Shade | -1.090 | -1.174 | -1.223 | -1.320 | -1.463 | -1.050 | -1.000 | | -1.463 | -1.000 | -1.189 | 39.0% | -1.162 | -1.162 | |
| 940-640 Mass, w/ Htg. Setback | -3.873 | -3.647 | -4.419 | -3.990 | -4.570 | -3.758 | -3.863 | -3.992 | -4.570 | -3.647 | -4.014 | 23.0% | -4.243 | -4.243 | |
| 950-650 Mass, w/ Night Vent | -4.429 | -4.614 | -5.257 | -4.973 | -5.956 | -4.537 | -4.558 | -4.685 | -5.956 | -4.429 | -4.876 | 31.3% | -4.981 | -4.981 | |
| PEAK HEATING [kW] | | | | | | | | | | Statistics for Example Results | | | | 10/26/2013 | GBS v3.4 |
| CASES | ESP DMU | BLAST US-IT | DOE21D NREL | SRES-SUN NREL | SRES BRE* | S3PAS SPAIN | TSYS BEL-BRE | TASE FINLAND | Min | Max | Mean | (Max-Min)/Mean** (%) | Autodesk | Autodesk | |
| 800-430 Mass, w/ Op. Win. | -0.215 | -0.151 | -0.141 | -0.149 | | -0.142 | -0.144 | -0.198 | -0.215 | -0.141 | -0.163 | 45.4% | -0.465 | -0.465 | |
| 900-800 Himass, S. Win. | -0.377 | -0.340 | -0.352 | -0.378 | | -0.294 | -0.269 | -0.142 | -0.378 | -0.142 | -0.307 | 76.7% | 0.138 | 0.138 | |
| 900-810 Himass, Int. Sol. Abs. | -0.129 | -0.113 | | -0.155 | | | -0.089 | -0.166 | -0.166 | -0.089 | -0.130 | 59.1% | 0.052 | 0.052 | |
| 910-610 Mass, w/ S. Shade | -0.579 | -0.485 | -0.470 | -0.494 | | -0.419 | -0.386 | -0.553 | -0.579 | -0.386 | -0.484 | 39.9% | -0.382 | -0.382 | |
| 920-620 Mass, w/ E&W Win. | -0.283 | -0.238 | -0.241 | -0.264 | | -0.248 | -0.214 | -0.318 | -0.318 | -0.214 | -0.258 | 40.4% | -0.279 | -0.279 | |
| 930-630 Mass w/ E&W Shade | -0.237 | -0.209 | -0.193 | -0.238 | | -0.214 | -0.178 | | -0.238 | -0.178 | -0.211 | 28.5% | -0.250 | -0.250 | |
| 940-640 Mass, w/ Htg. Setback | -1.252 | -0.458 | -0.278 | -0.414 | | -0.230 | -0.600 | -0.526 | -1.252 | -0.230 | -0.537 | 190.4% | 0.074 | 0.074 | |
| PEAK SENSIBLE COOLING [kW] | | | | | | | | | | Statistics for Example Results | | | | 10/26/2013 | GBS v3.4 |
| CASES | ESP DMU | BLAST US-IT | DOE21D NREL | SRES-SUN NREL | SRES BRE* | S3PAS SPAIN | TSYS BEL-BRE | TASE FINLAND | Min | Max | Mean | (Max-Min)/Mean** (%) | Autodesk | Autodesk | |
| 800-430 Mass, w/ Op. Win. | -0.908 | -0.805 | -0.684 | -0.410 | | -0.547 | -0.816 | -1.220 | -1.220 | -0.410 | -0.770 | 105.2% | -1.311 | -1.311 | |
| 900-800 Himass, S. Win. | 2.303 | 2.188 | 2.715 | 2.519 | | 2.306 | 2.584 | 2.099 | 2.099 | 2.715 | 2.388 | 25.8% | 2.905 | 2.905 | |
| 900-810 Himass, Int. Sol. Abs. | 1.036 | 0.798 | | 0.880 | | | 1.223 | 0.595 | 0.595 | 1.223 | 0.906 | 69.3% | 1.116 | 1.116 | |
| 910-610 Mass, w/ S. Shade | -3.773 | -3.324 | -3.728 | -3.094 | | -3.384 | -2.883 | -2.999 | -3.773 | -2.883 | -3.312 | 26.9% | -3.107 | -3.107 | |
| 920-620 Mass, w/ E&W Win. | -1.249 | -1.142 | -1.321 | -1.106 | | -1.226 | -1.225 | -1.591 | -1.591 | -1.106 | -1.266 | 38.3% | -1.159 | -1.159 | |
| 930-630 Mass w/ E&W Shade | -1.199 | -1.158 | -1.200 | -1.036 | | -1.179 | -1.110 | | -1.200 | -1.036 | -1.147 | 14.3% | -1.060 | -1.060 | |
| 940-640 Mass, w/ Htg. Setback | -3.273 | -2.737 | -3.118 | -2.905 | | -2.916 | -2.875 | -3.314 | -3.314 | -2.737 | -3.020 | 19.1% | -2.914 | -2.914 | |
| 950-650 Mass, w/ Night Vent | -3.998 | -3.210 | -3.852 | -3.501 | | -3.466 | -3.692 | -3.812 | -3.998 | -3.210 | -3.647 | 21.6% | -3.310 | -3.310 | |

* SRES-BRE (SERIRES 1.2) simulations did not produce output for this variable.

** ABS[(Max-Min) / (Mean of Example Simulation Results)]

**ASHRAE Standard 140-2011 Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Tests
Autodesk Green Building Studio 10/26/2013 vs. Annex B8, Section B8.1 Example Results
By Autodesk , 26-Oct-2013**

Note: The statistics in the tables below are based on the Standard 140 informative example results.
These statistics do not have any substantial importance and are not to be interpreted as acceptance criteria.

Table B8-11. Annual Transmissivity Coefficient of Windows

(ANNUAL UNSHADED TRANSMITTED SOLAR RADIATION)/(ANNUAL UNSHADED INCIDENT SOLAR RADIATION)

| Simulation Model: Organization or Country: Case | ESP DMU | DOE21D NREL | SRES-SUN NREL | SRES BRE | S3PAS SPAIN | TSYS BEL-BRE | TASE FINLAND | Statistics for Example Results | | | | GBS 10/26/2013 Autodesk | GBS v3.4 Autodesk |
|---|------------|----------------|------------------|-------------|----------------|-----------------|-----------------|--------------------------------|-------|-------|-------------------------|----------------------------|----------------------|
| | | | | | | | | Min | Max | Mean | (Max-Min)/ Mean* (%) | | |
| 620 West | 0.674 | 0.681 | 0.687 | 0.657 | 0.641 | 0.654 | 0.648 | 0.641 | 0.687 | 0.663 | 7.0% | 0.799 | 0.799 |
| 600 South | 0.650 | 0.671 | 0.652 | 0.650 | 0.628 | 0.647 | 0.623 | 0.623 | 0.671 | 0.646 | 7.5% | 0.791 | 0.791 |

* ABS[(Max-Min) / (Mean of Example Simulation Results)]

Table B8-12. Annual Shading Coefficient of Window Shading Devices: Overhangs & Fins

(1-(ANNUAL SHADED TRANSMITTED SOLAR RADIATION))/(ANNUAL UNSHADED TRANSMITTED SOLAR RADIATION)

| Simulation Model: Organization or Country: Case | ESP DMU | DOE21D NREL | SRES-SUN NREL | SRES BRE | S3PAS SPAIN | TSYS BEL-BRE | TASE FINLAND | Statistics for Example Results | | | | GBS 10/26/2013 Autodesk | GBS v3.4 Autodesk |
|---|------------|----------------|------------------|-------------|----------------|-----------------|-----------------|--------------------------------|-------|-------|-------------------------|----------------------------|----------------------|
| | | | | | | | | Min | Max | Mean | (Max-Min)/ Mean* (%) | | |
| 630/620 West | 0.182 | 0.346 | 0.196 | 0.216 | 0.329 | 0.339 | | 0.182 | 0.346 | 0.268 | 61.2% | 0.377 | 0.377 |
| 610/600 South | 0.170 | 0.209 | 0.165 | 0.188 | 0.183 | 0.205 | 0.115 | 0.115 | 0.209 | 0.177 | 53.5% | 0.209 | 0.209 |

* ABS[(Max-Min) / (Mean of Example Simulation Results)]

Table B8-13. Case 600 Annual Incident Solar Radiation (kWh/m²)

| Simulation Model: Organization or Country: Case | ESP DMU | DOE21D NREL | SRES-SUN NREL | SRES BRE | S3PAS SPAIN | TSYS BEL-BRE | TASE FINLAND | Statistics for Example Results | | | | GBS 10/26/2013 Autodesk | GBS v3.4 Autodesk |
|---|------------|----------------|------------------|-------------|----------------|-----------------|-----------------|--------------------------------|------|------|-------------------------|----------------------------|----------------------|
| | | | | | | | | Min | Max | Mean | (Max-Min)/ Mean* (%) | | |
| North | 427 | 434 | 456 | 407 | 457 | 367 | 453 | 367 | 457 | 429 | 20.9% | 450 | 450 |
| East | 959 | 1155 | 1083 | 1217 | 1082 | 1101 | 962 | 959 | 1217 | 1080 | 23.9% | 1167 | 1167 |
| West | 1086 | 1079 | 1003 | 857 | 1002 | 1012 | 1090 | 857 | 1090 | 1018 | 22.9% | 1092 | 1092 |
| South | 1456 | 1566 | 1476 | 1468 | 1474 | 1522 | 1468 | 1456 | 1566 | 1490 | 7.4% | 1577 | 1577 |
| Horizontal | 1797 | 1831 | 1832 | 1832 | 1832 | 1832 | 1832 | 1797 | 1832 | 1827 | 1.9% | 1832 | 1832 |

* ABS[(Max-Min) / (Mean of Example Simulation Results)]

**ASHRAE Standard 140-2011 Test Results Comparison for Section 5.2 - Building Thermal Envelope and Fabric Load Tests
Autodesk Green Building Studio 10/26/2013 vs. Annex B8, Section B8.1 Example Results
By Autodesk , 26-Oct-2013**

Note: The statistics in the tables below are based on the Standard 140 informative example results.
These statistics do not have any substantial importance and are not to be interpreted as acceptance criteria.

Table B8-14. Case 600 Annual Transmitted Solar Radiation - Unshaded (kWh/m²)

| Simulation Model: Organization or Country: | ESP DMU | DOE21D NREL | SRES-SUN NREL | SRES BRE | S3PAS SPAIN | TSYS BEL-BRE | TASE FINLAND | Statistics for Example Results | | | | GBS 10/26/2013 Autodesk | GBS v3.4 Autodesk |
|---|------------|----------------|------------------|-------------|----------------|-----------------|-----------------|--------------------------------|------|------|-------------------------|----------------------------|----------------------|
| | | | | | | | | Min | Max | Mean | (Max-Min)/ Mean* (%) | | |
| Case | | | | | | | | | | | | | |
| West | 732 | 735 | 689 | 563 | 642 | 662 | 706 | 563 | 735 | 676 | 25.5% | 872 | 872 |
| South | 946 | 1051 | 962 | 954 | 926 | 984 | 914 | 914 | 1051 | 962 | 14.2% | 1247 | 1247 |

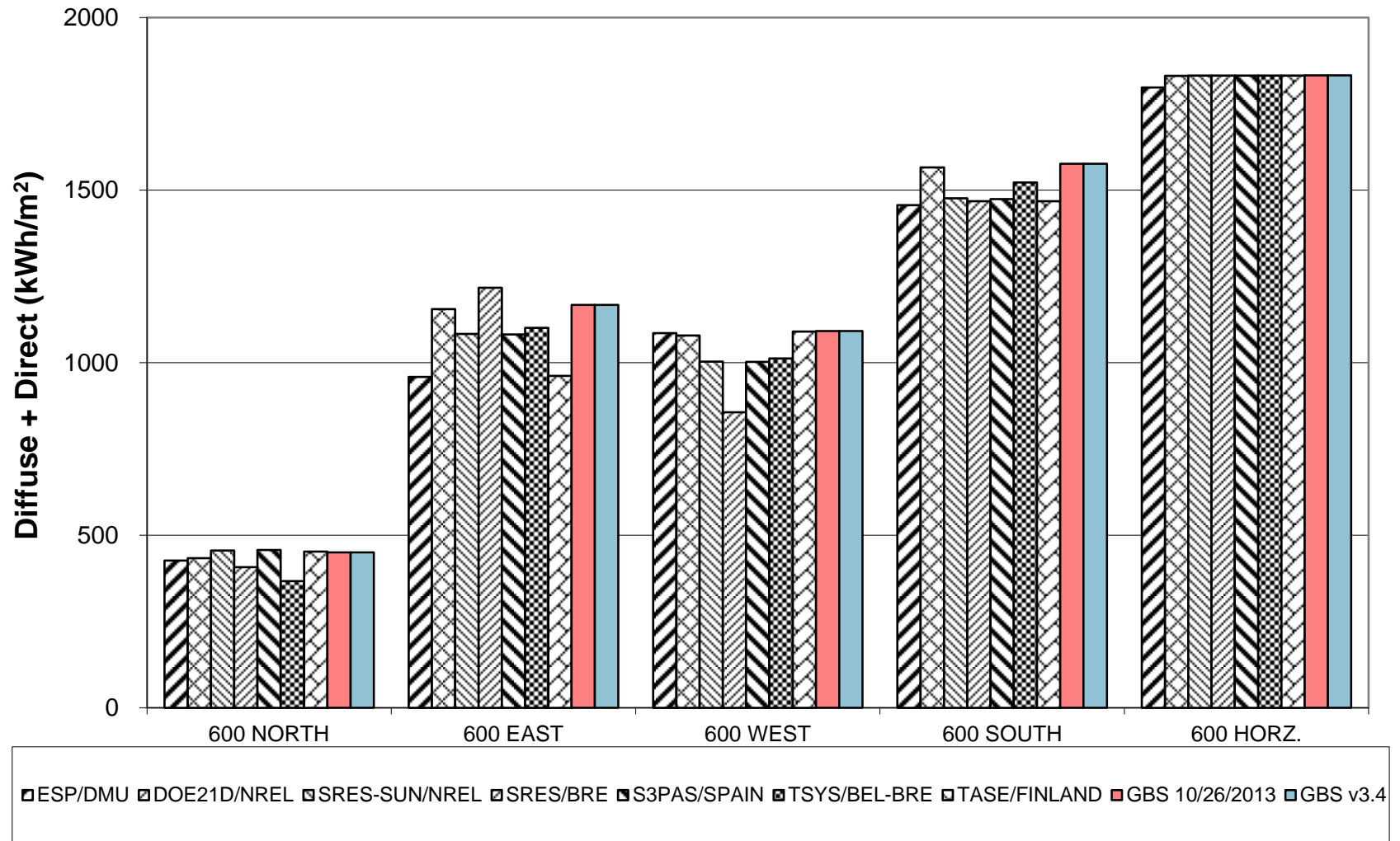
* ABS[(Max-Min) / (Mean of Example Simulation Results)]

Table B8-15. Case 600 Annual Transmitted Solar Radiation - Shaded (kWh/m²)

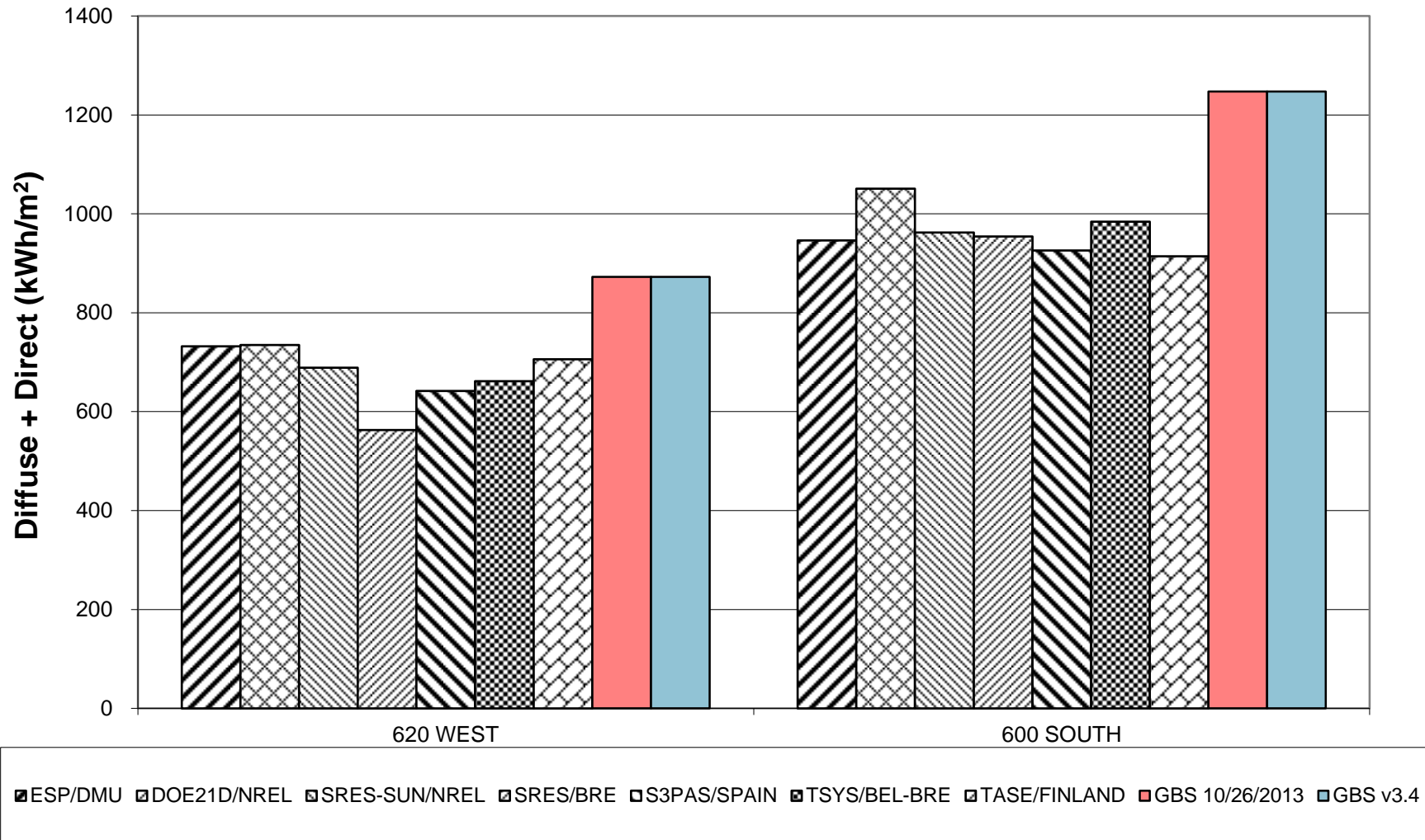
| Simulation Model: Organization or Country: | ESP DMU | DOE21D NREL | SRES-SUN NREL | SRES BRE | S3PAS SPAIN | TSYS BEL-BRE | TASE FINLAND | Statistics for Example Results | | | | GBS 10/26/2013 Autodesk | GBS v3.4 Autodesk |
|---|------------|----------------|------------------|-------------|----------------|-----------------|-----------------|--------------------------------|-----|------|-------------------------|----------------------------|----------------------|
| | | | | | | | | Min | Max | Mean | (Max-Min)/ Mean* (%) | | |
| Case | | | | | | | | | | | | | |
| West | 599 | 481 | 554 | 441 | 431 | 438 | | 431 | 599 | 491 | 34.2% | 543 | 543 |
| South | 785 | 831 | 803 | 775 | 757 | 782 | 809 | 757 | 831 | 792 | 9.3% | 986 | 986 |

* ABS[(Max-Min) / (Mean of Example Simulation Results)]

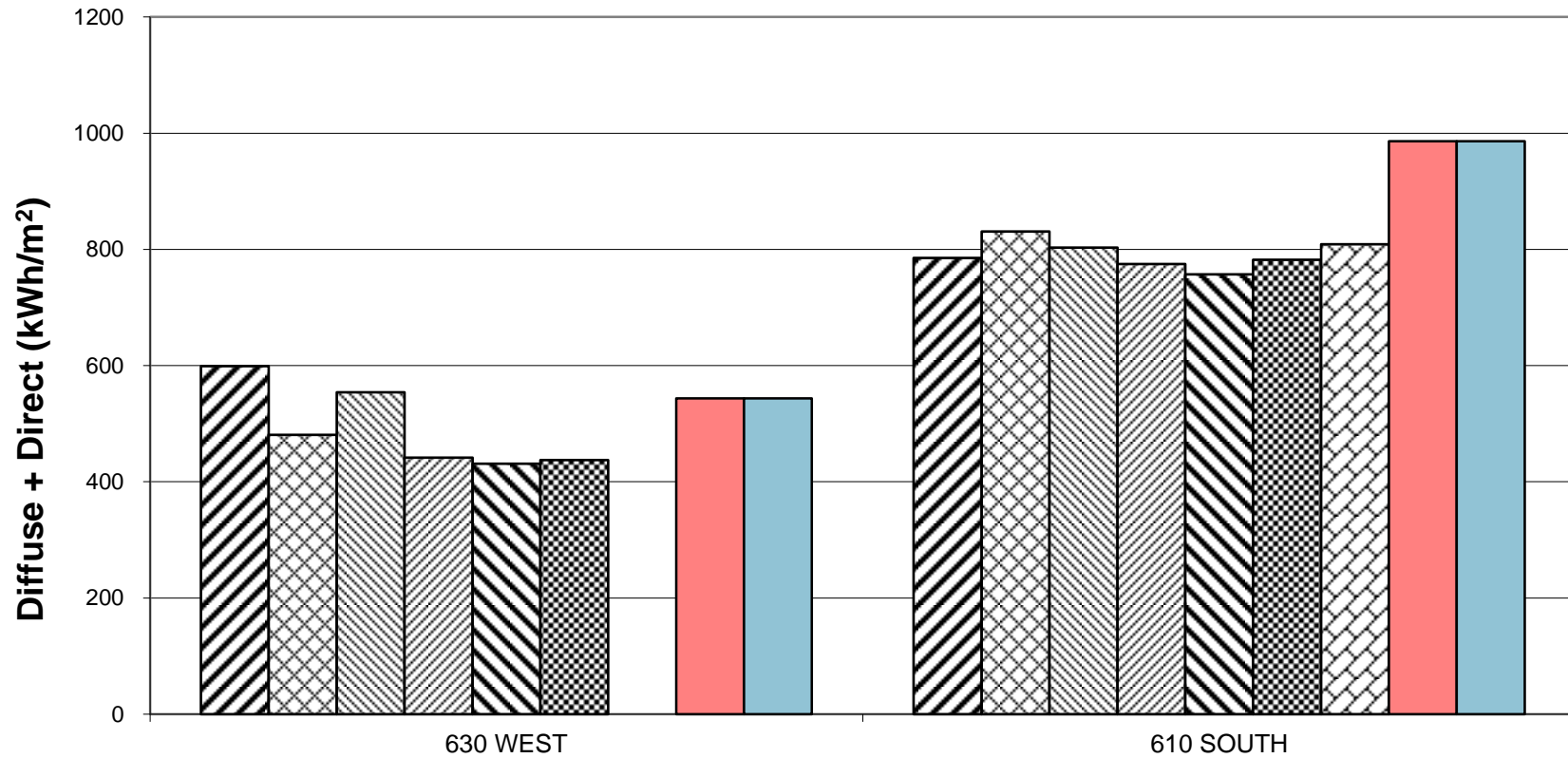
**Figure B8-1. BESTEST BASIC
 Annual Incident Solar Radiation**



**Figure B8-2. BESTEST BASIC
 Annual Transmitted Solar Radiation - Unshaded**



**Figure B8-3. BESTEST BASIC
 Annual Transmitted Solar Radiation - Shaded**



| | | | | |
|--------------|--------------|----------------|----------|-------------|
| ESP/DMU | DOE21D/NREL | SRES-SUN/NREL | SRES/BRE | S3PAS/SPAIN |
| TSYS/BEL-BRE | TASE/FINLAND | GBS 10/26/2013 | GBS v3.4 | |

Figure B8-4. BESTEST BASIC
Annual Transmissivity Coefficient of Windows
(Unshaded Transmitted)/(Incident Solar Radiation)

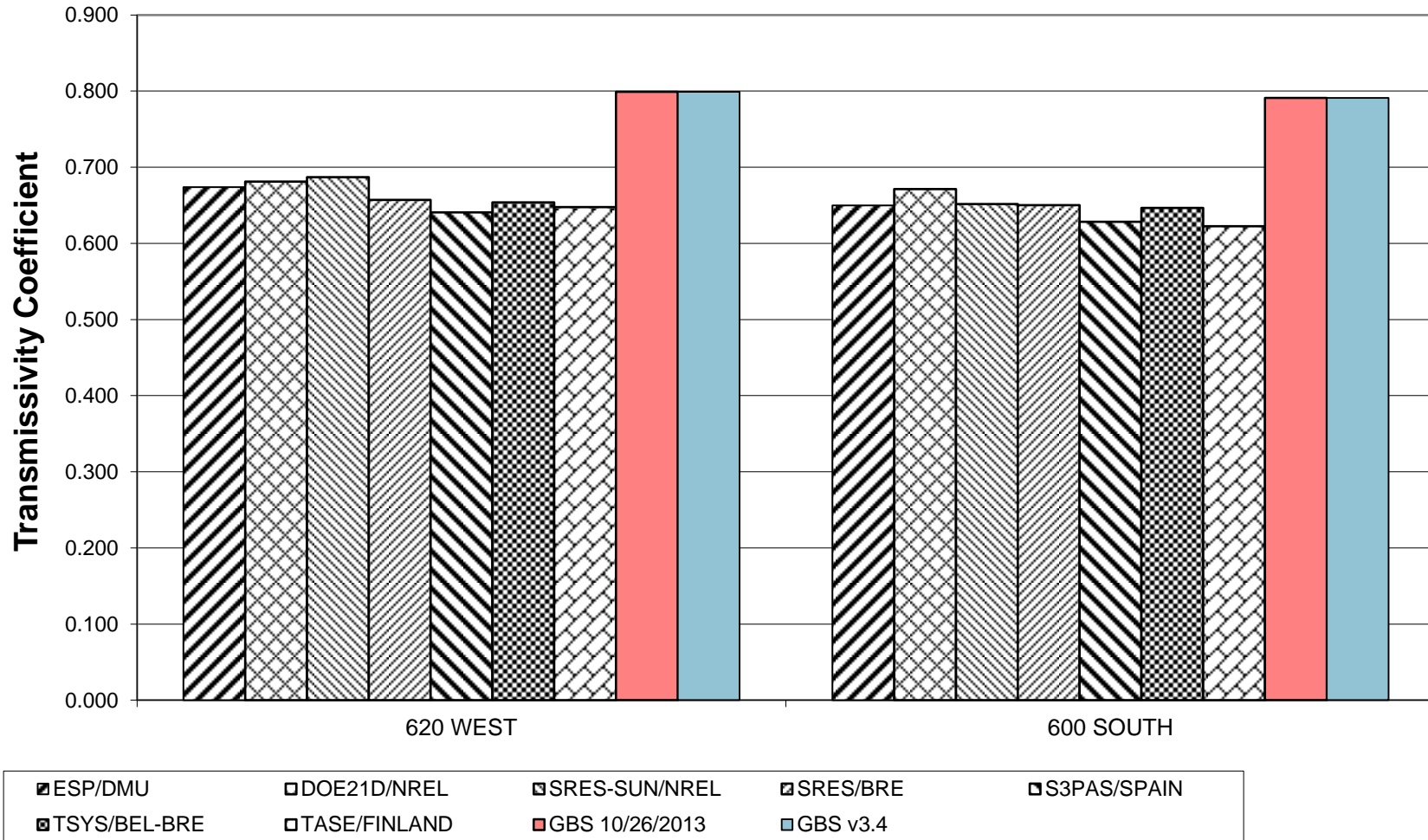
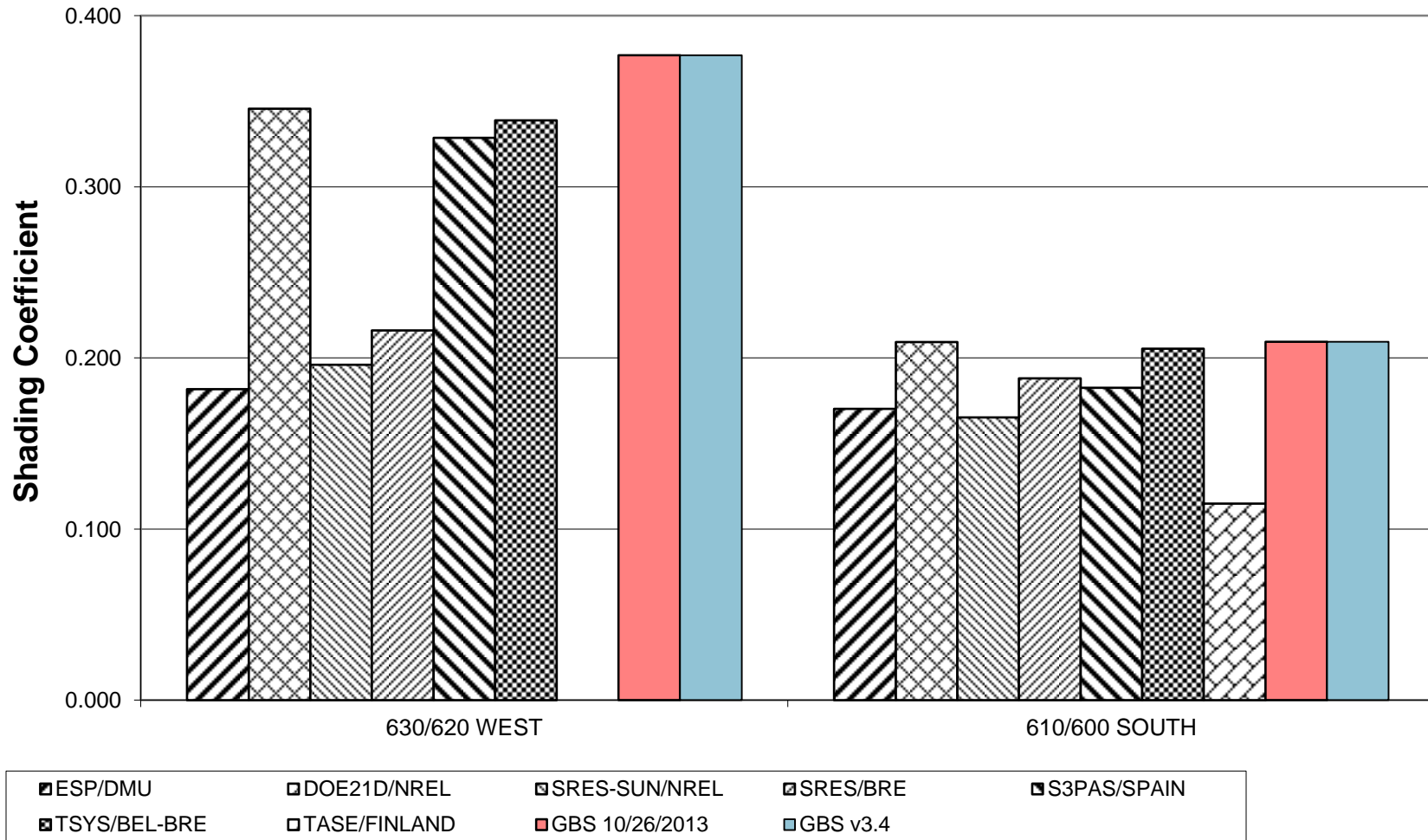
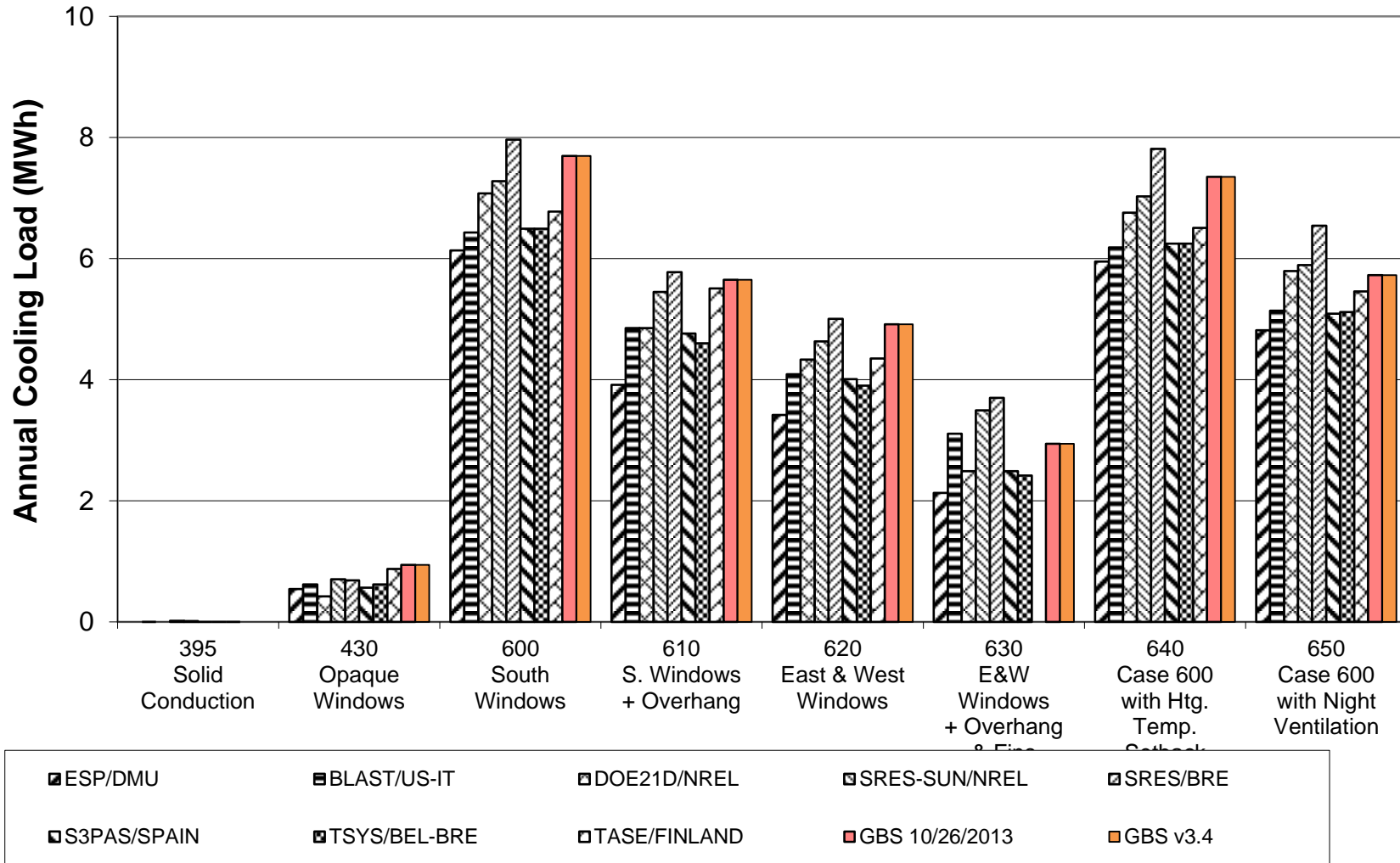


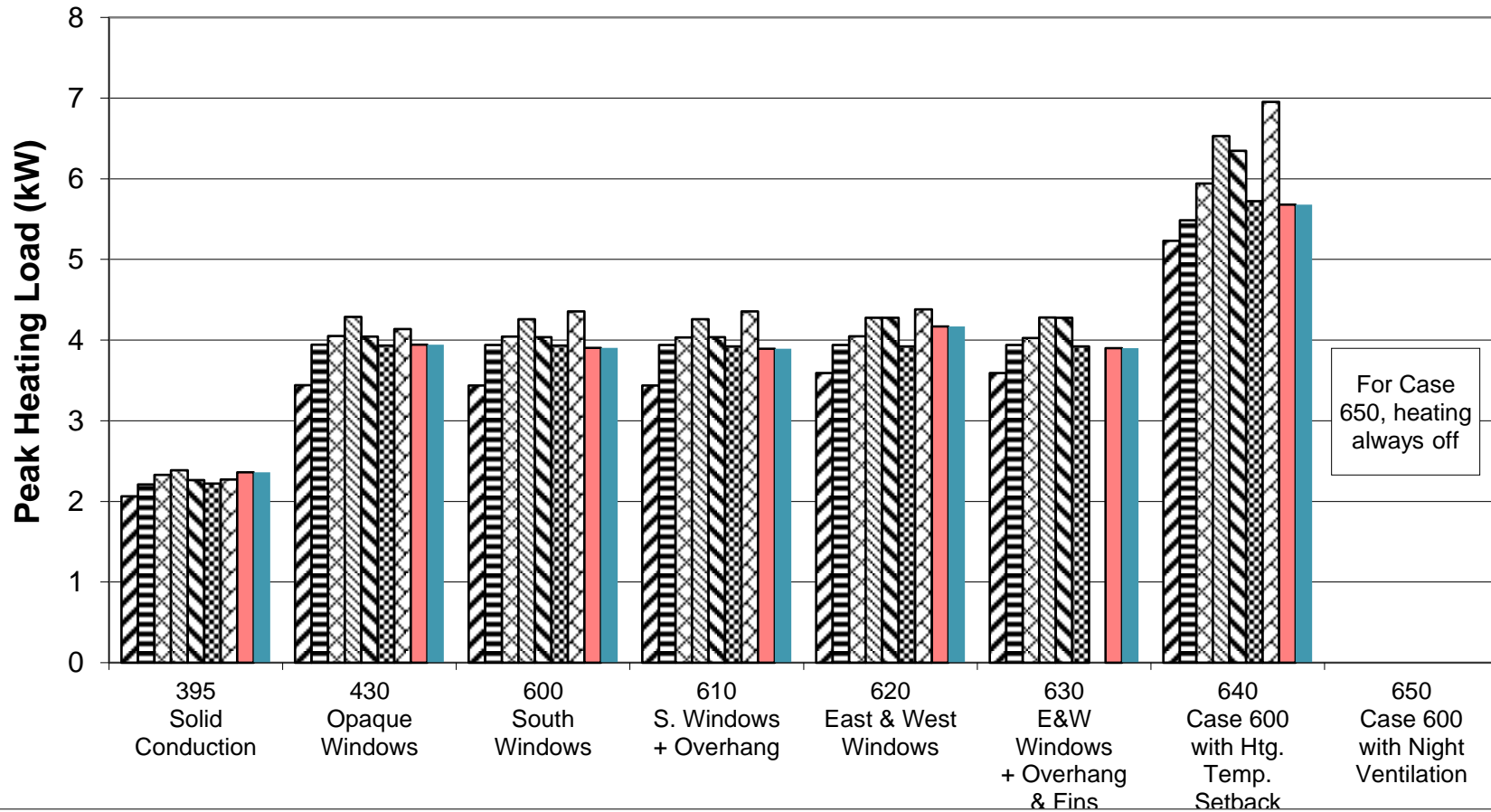
Figure B8-5. BESTEST BASIC
Annual Overhang and Fin Shading Coefficients
(1-(Shaded)/(Unshaded)) Transmitted Solar Radiation



**Figure B8-7. BESTEST BASIC
 Low Mass Annual Sensible Cooling**

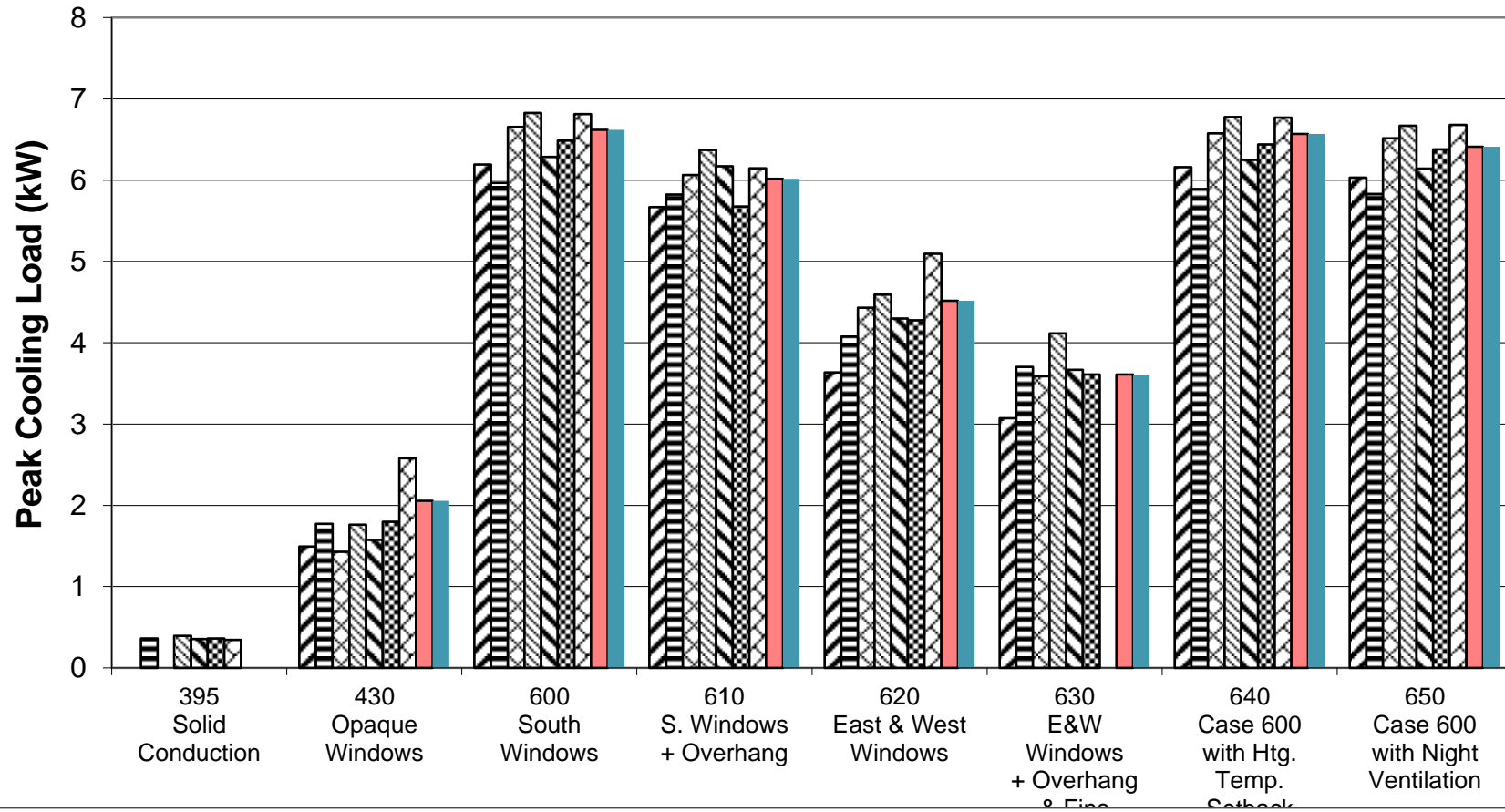


**Figure B8-8. BESTEST BASIC
 Low Mass Peak Heating**



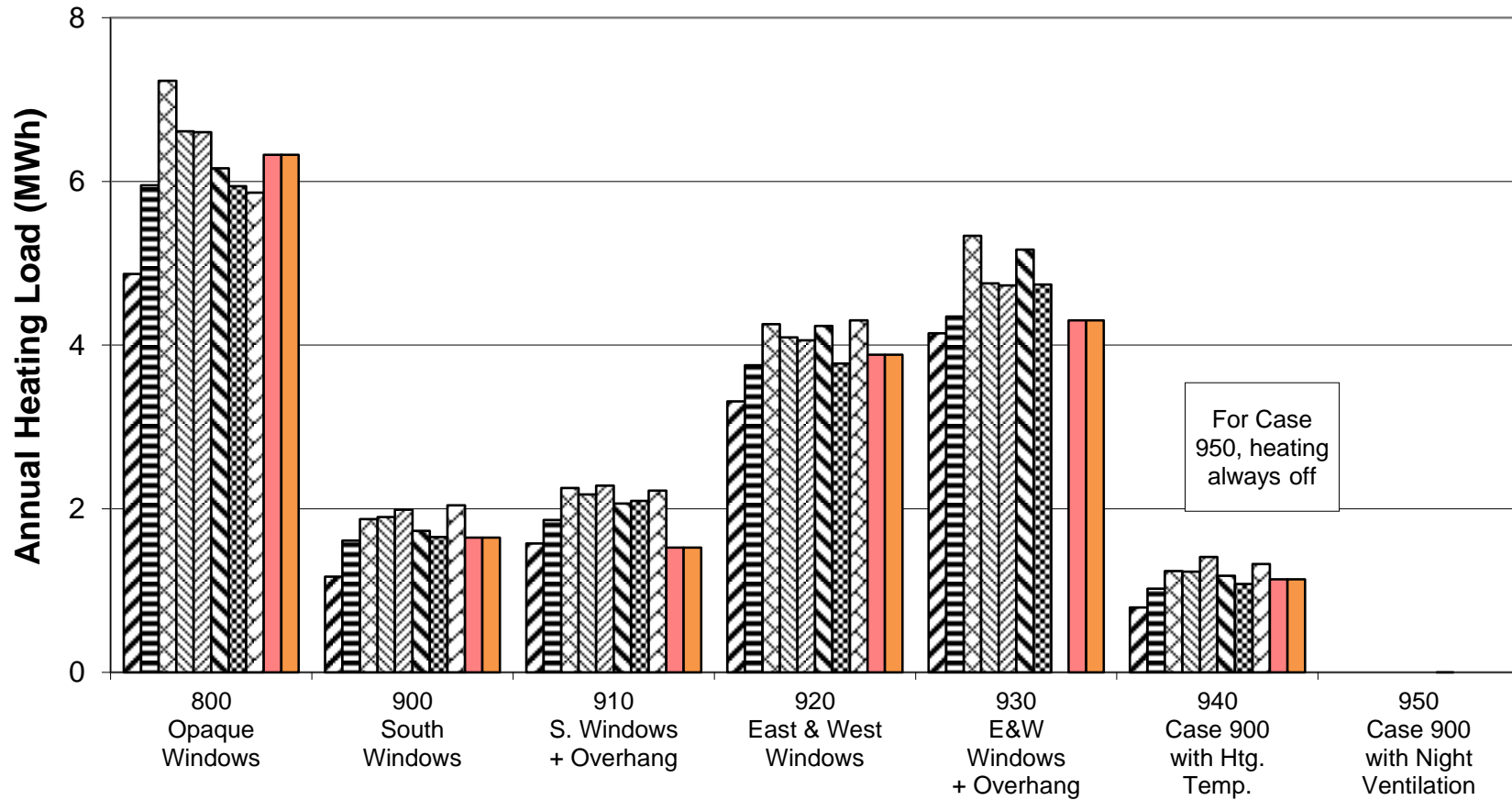
ESP/DMU
 BLAST/US-IT
 DOE21D/NREL
 SRES-SUN/NREL
 S3PAS/SPAIN
 TSYS/BEL-BRE
 TASE/FINLAND
 GBS 10/26/2013
 GBS v3.4

**Figure B8-9. BESTEST BASIC
 Low Mass Peak Sensible Cooling**



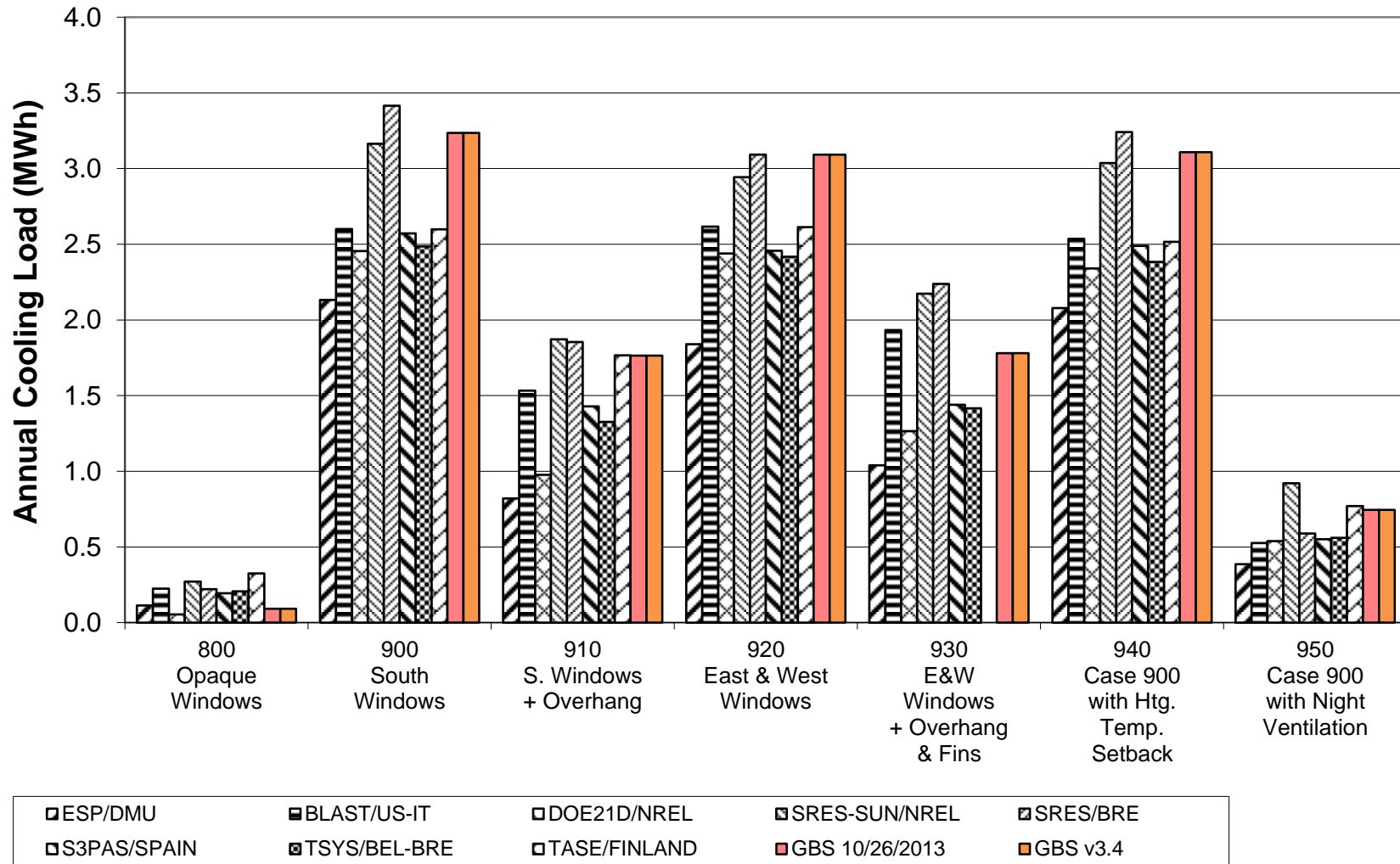
ESP/DMU
 BLAST/US-IT
 DOE21D/NREL
 SRES-SUN/NREL
 S3PAS/SPAIN
 TSYS/BEL-BRE
 TASE/FINLAND
 GBS 10/26/2013
 GBS v3.4

**Figure B8-10. BESTEST BASIC
High Mass Annual Heating**

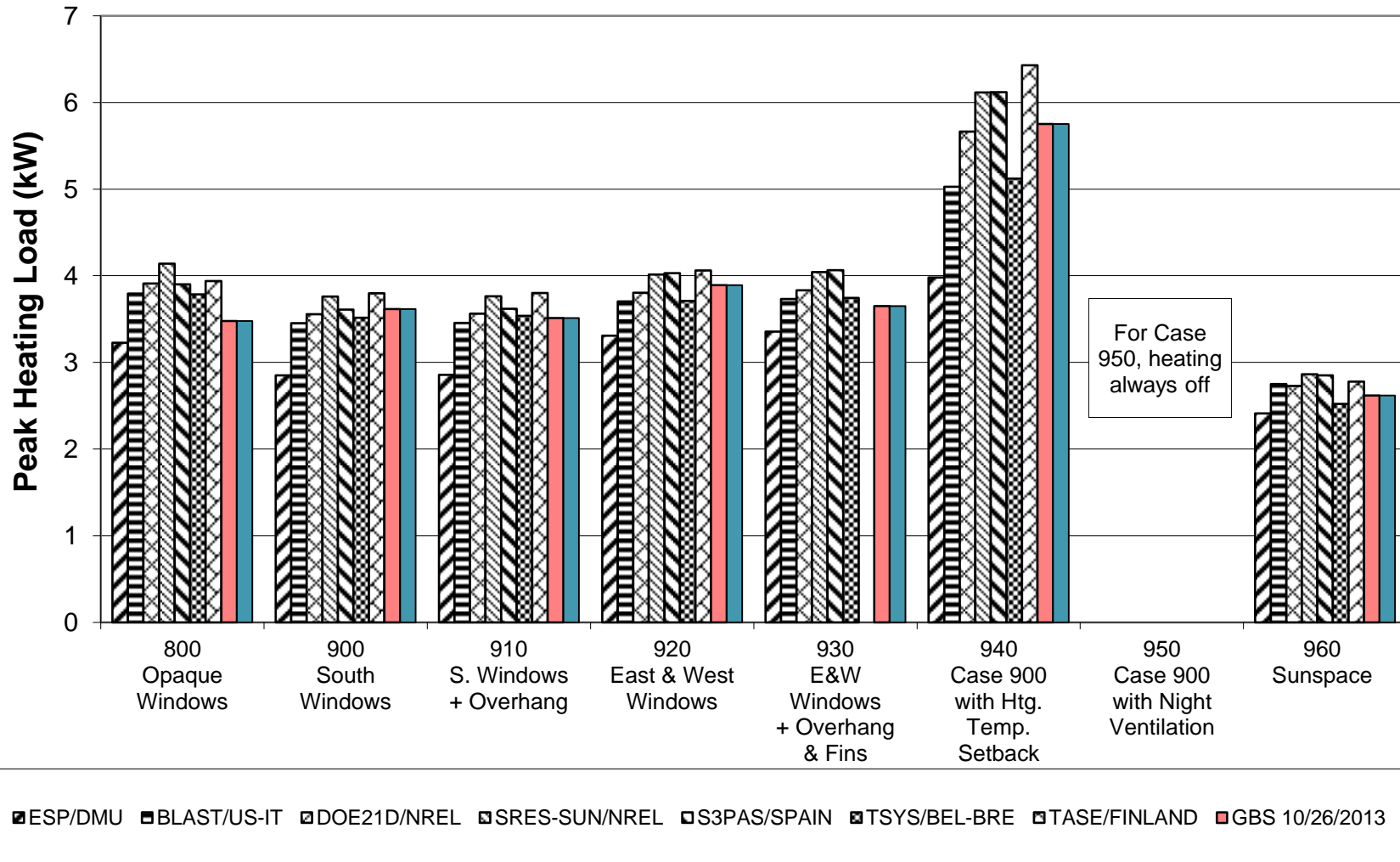


| | | | | |
|-------------|--------------|--------------|----------------|----------|
| ESP/DMU | BLAST/US-IT | DOE21D/NREL | SRES-SUN/NREL | SRES/BRE |
| S3PAS/SPAIN | TSYS/BEL-BRE | TASE/FINLAND | GBS 10/26/2013 | GBS v3.4 |

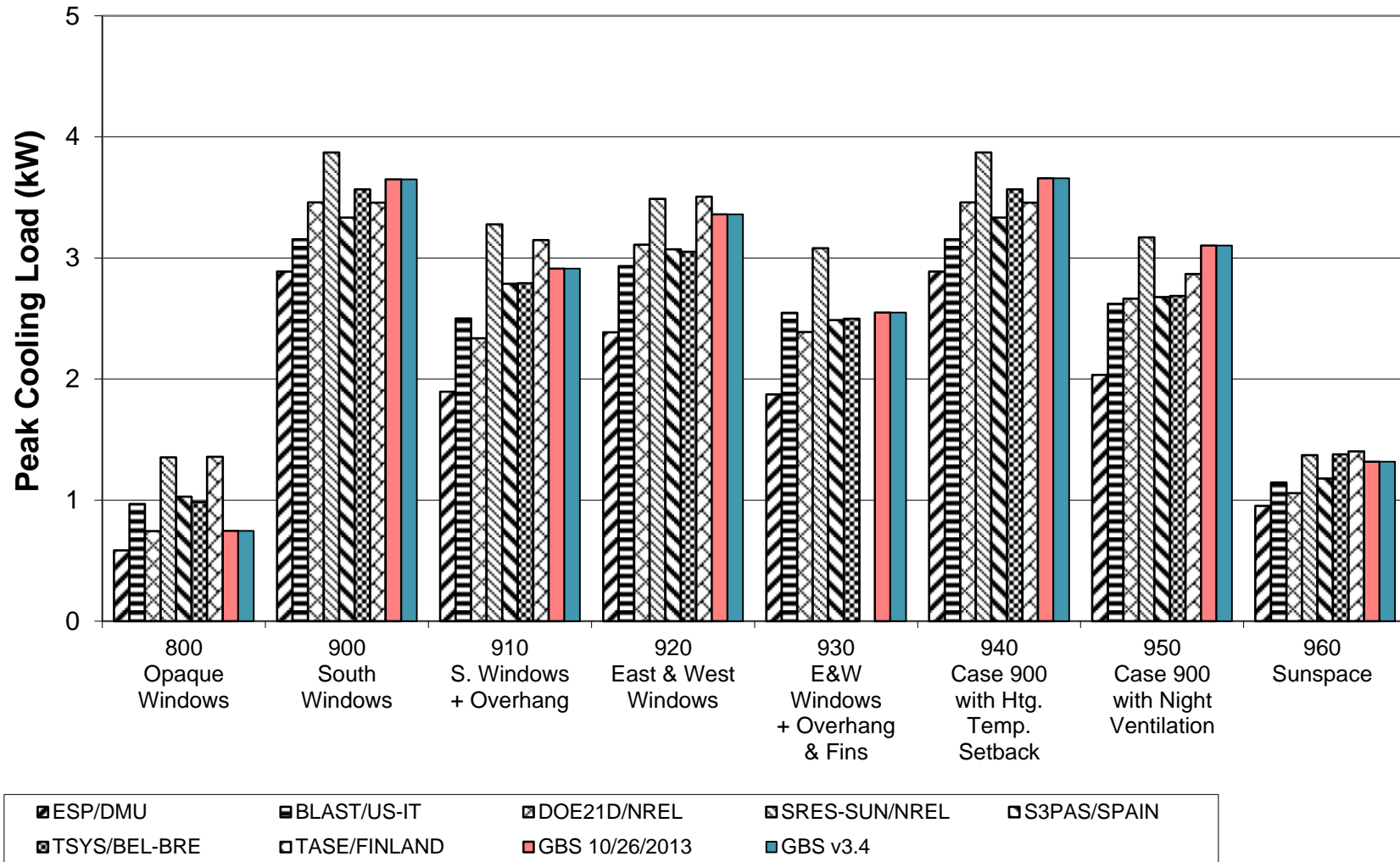
**Figure B8-11. BESTEST BASIC
 High Mass Annual Sensible Cooling**



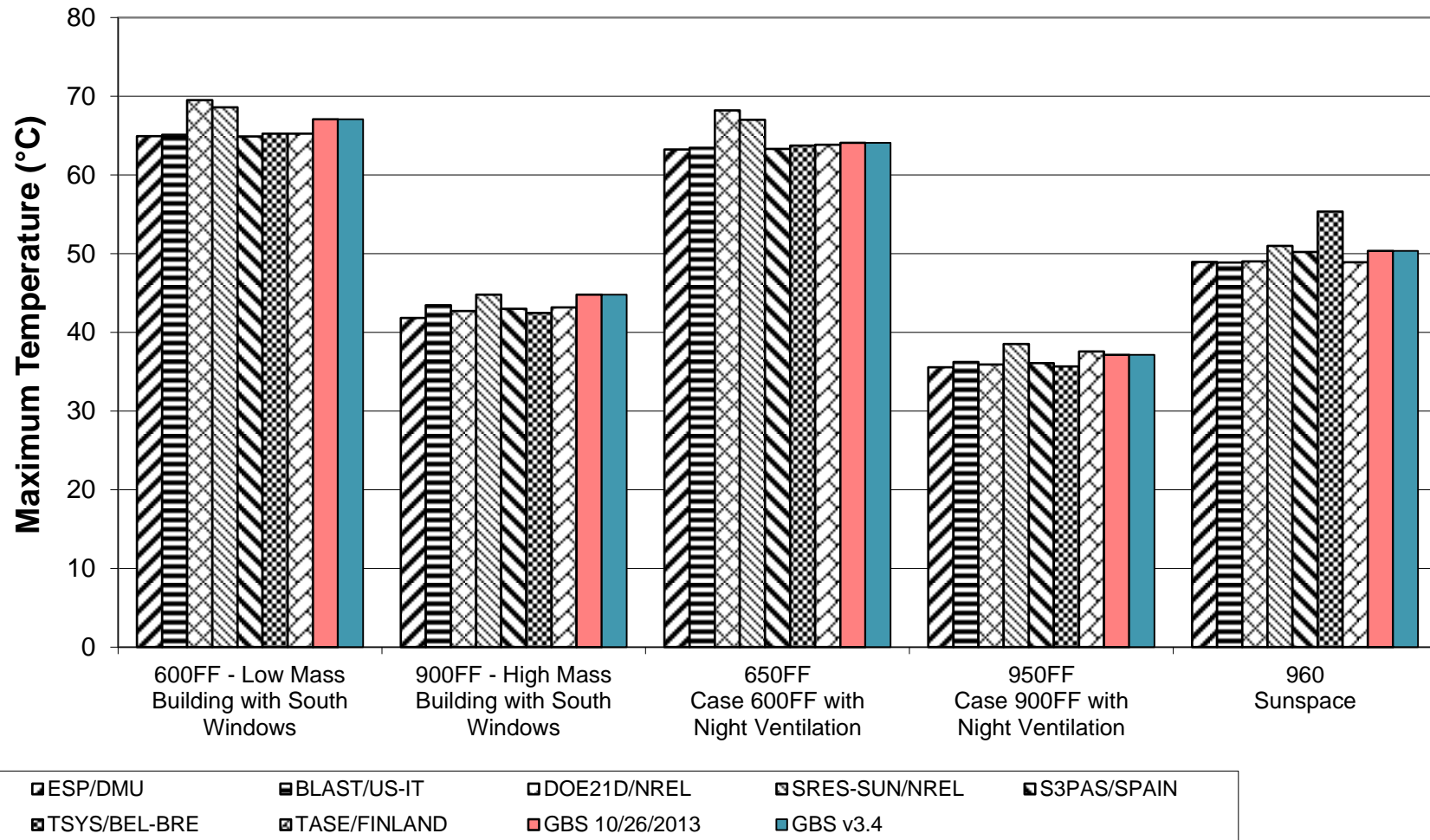
**Figure B8-12. BESTEST BASIC
 High Mass Peak Heating**



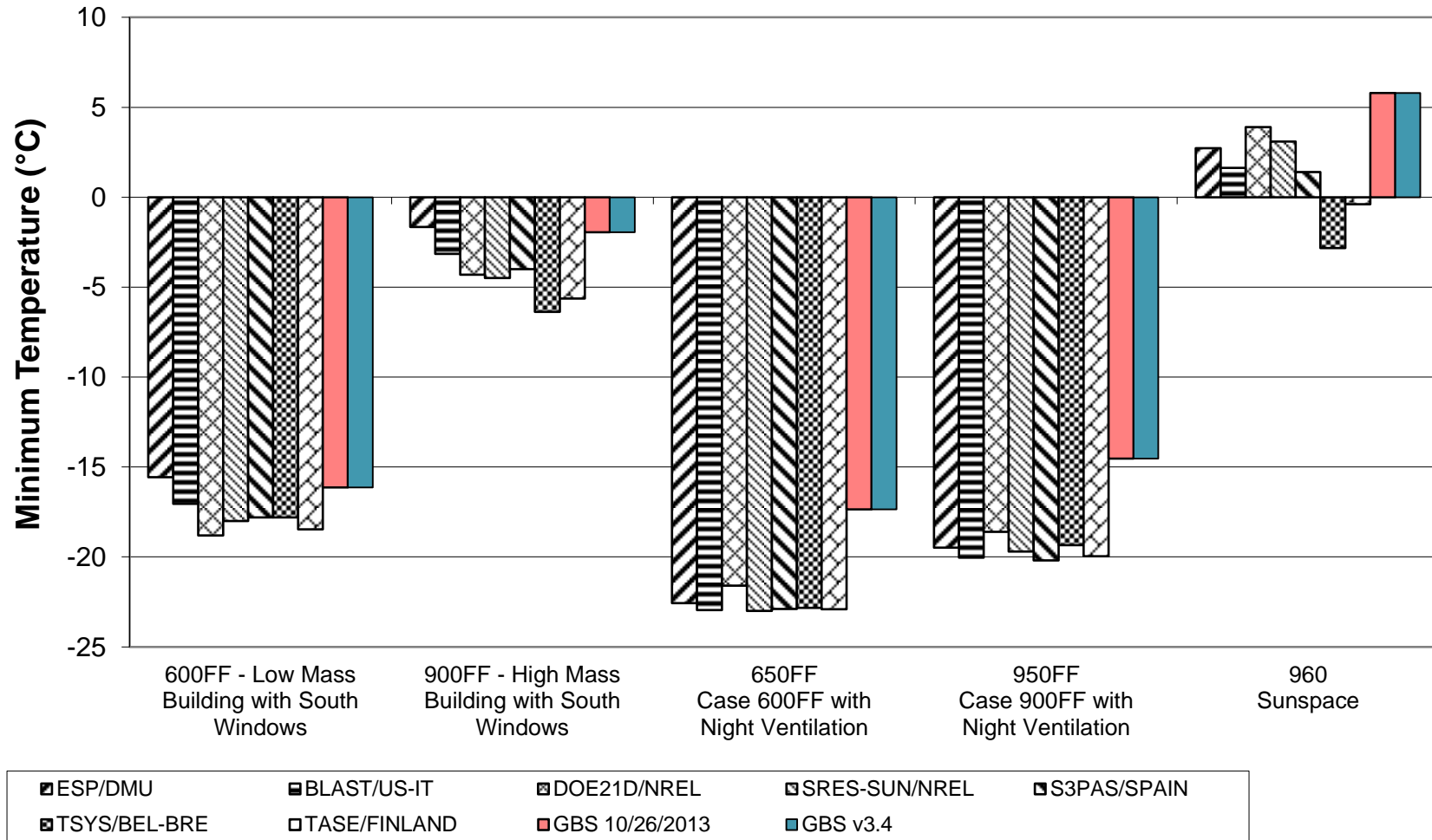
**Figure B8-13. BESTEST BASIC
 High Mass Peak Sensible Cooling**



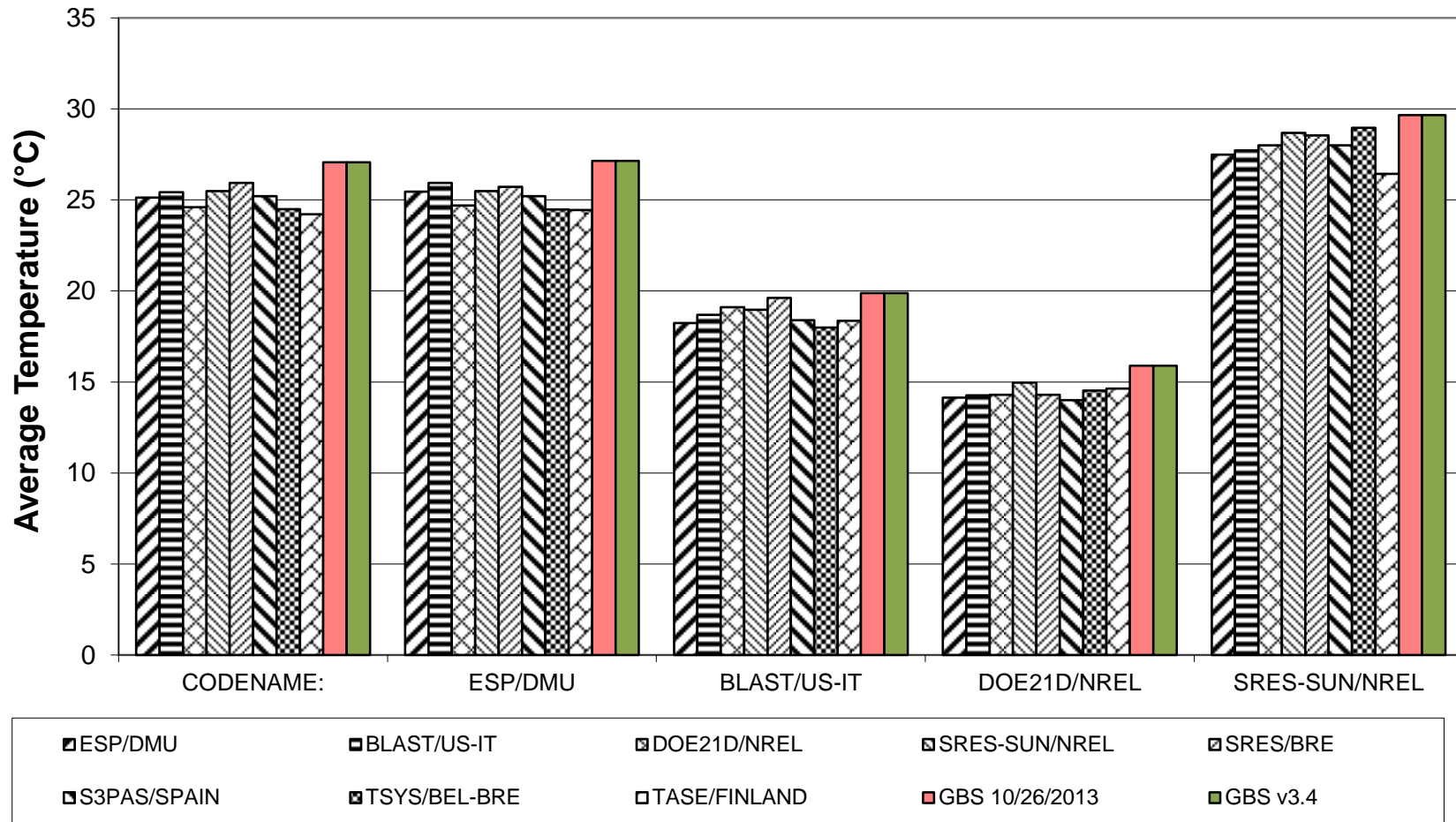
**Figure B8-14. BESTEST BASIC
Maximum Hourly Annual Temperature
Free-Float Cases**



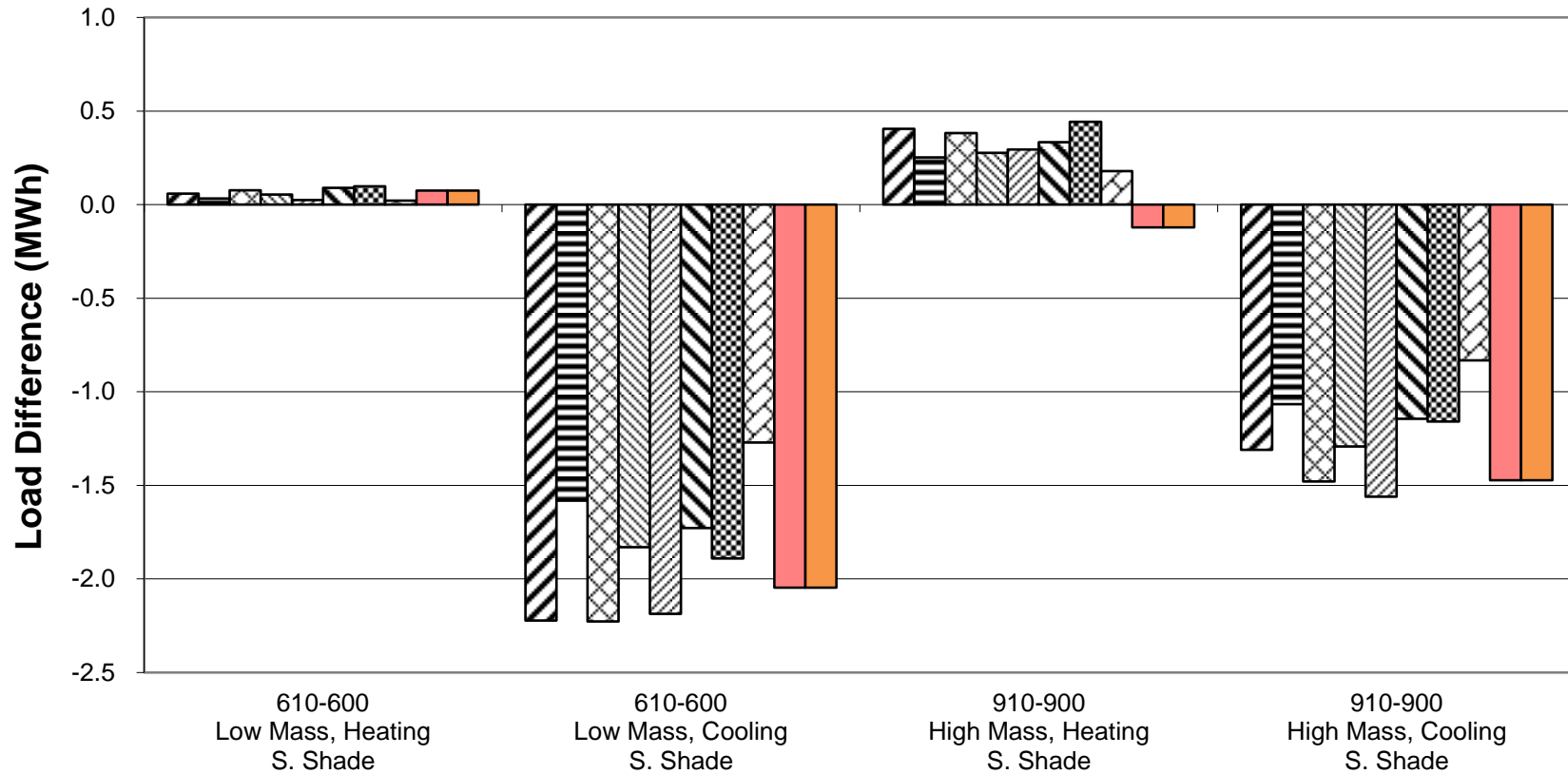
**Figure B8-15. BESTEST BASIC
Minimum Hourly Annual Temperature
Free-Float Cases**



**Figure B8-16. BESTEST BASIC
 Average Hourly Annual Temperature
 Free-Float Cases**

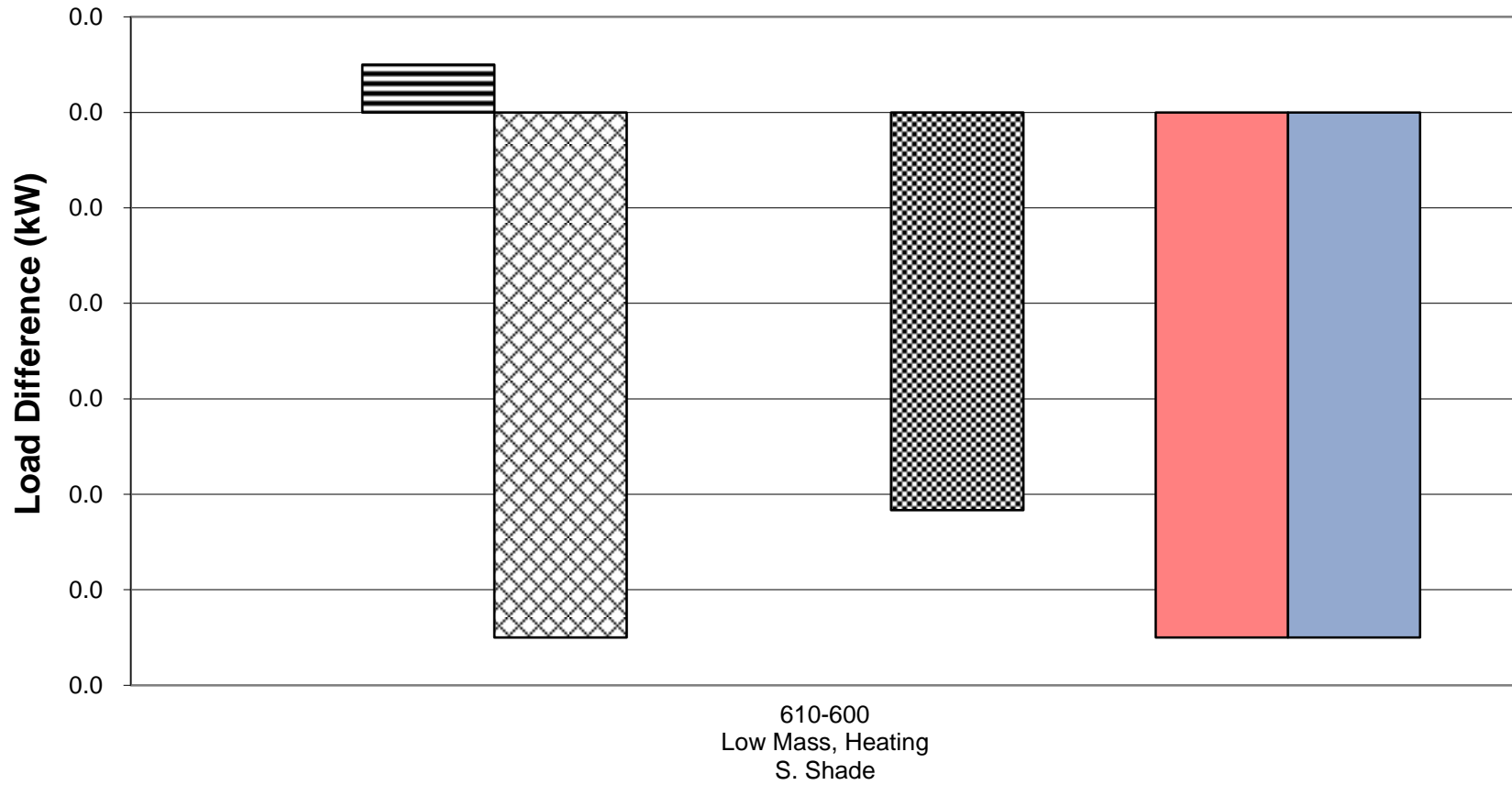


**Figure B8-17. BESTEST BASIC
 South Window Shading (Delta)
 Annual Heating and Sensible Cooling**



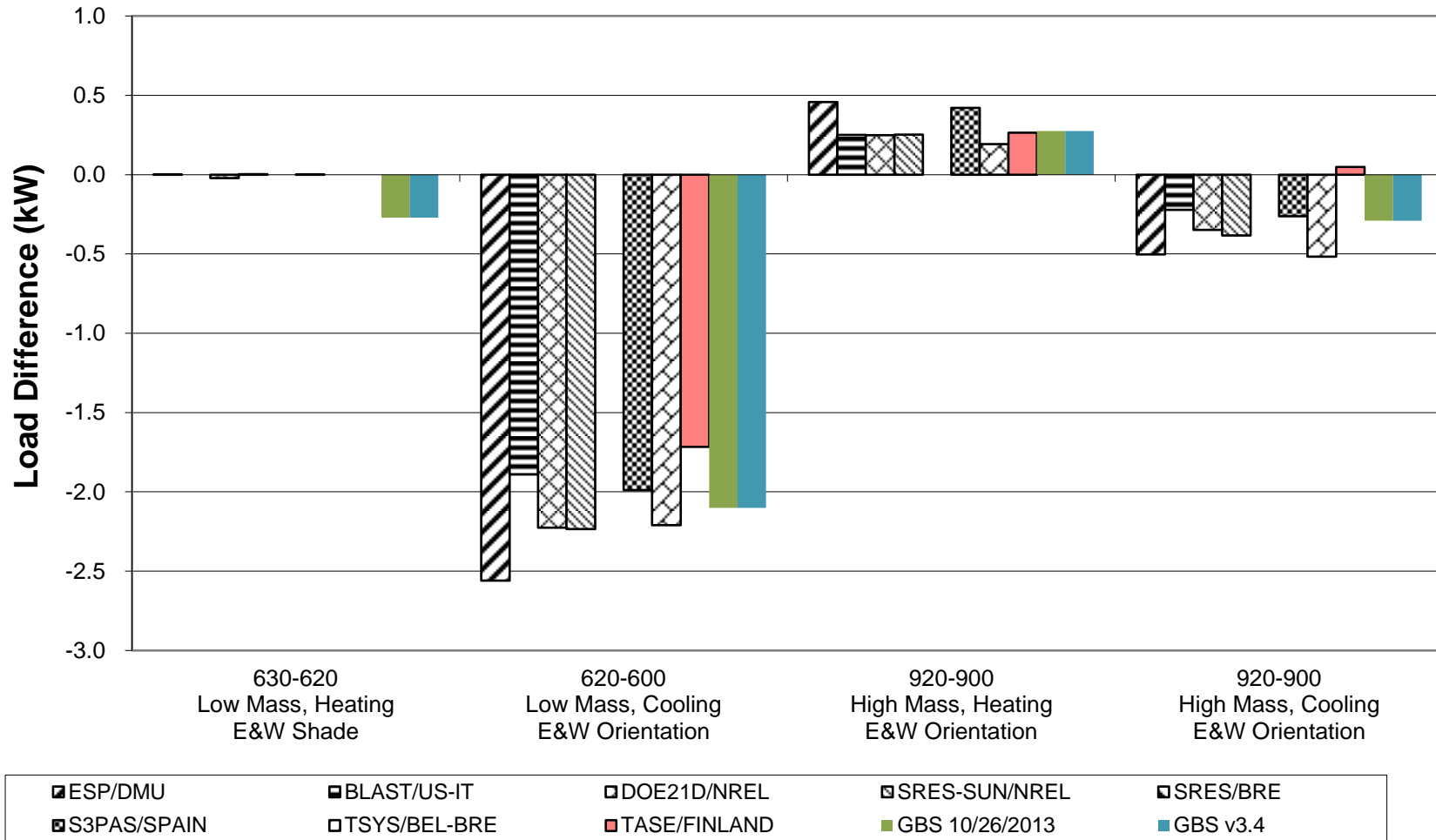
| | | | | |
|-------------|--------------|--------------|----------------|----------|
| ESP/DMU | BLAST/US-IT | DOE21D/NREL | SRES-SUN/NREL | SRES/BRE |
| S3PAS/SPAIN | TSYS/BEL-BRE | TASE/FINLAND | GBS 10/26/2013 | GBS v3.4 |

**Figure B8-18. BESTEST BASIC
 South Window Shading (Delta)
 Peak Heating and Sensible Cooling**

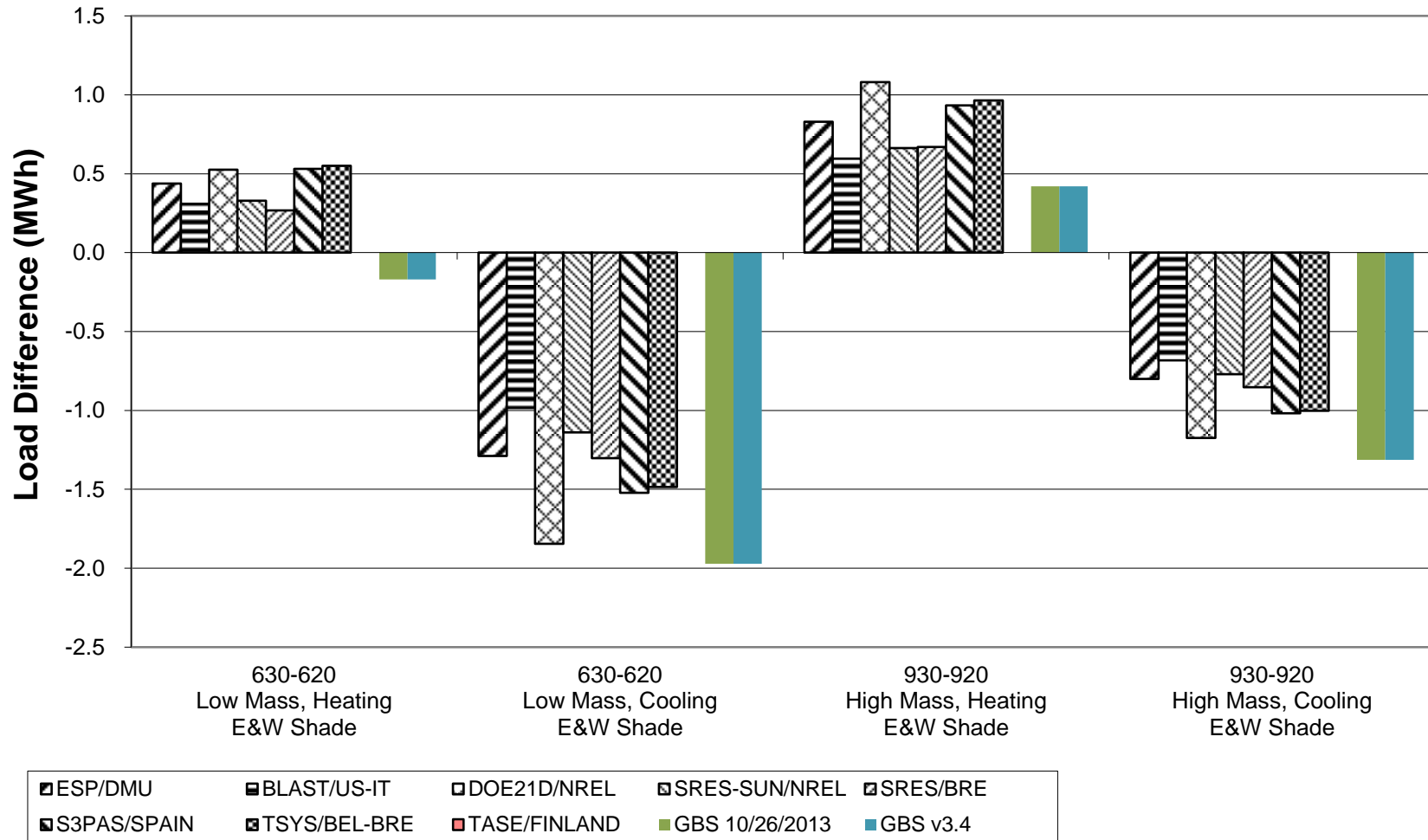


| | | | | |
|--------------|--------------|----------------|---------------|-------------|
| ESP/DMU | BLAST/US-IT | DOE21D/NREL | SRES-SUN/NREL | S3PAS/SPAIN |
| TSYS/BEL-BRE | TASE/FINLAND | GBS 10/26/2013 | GBS v3.4 | |

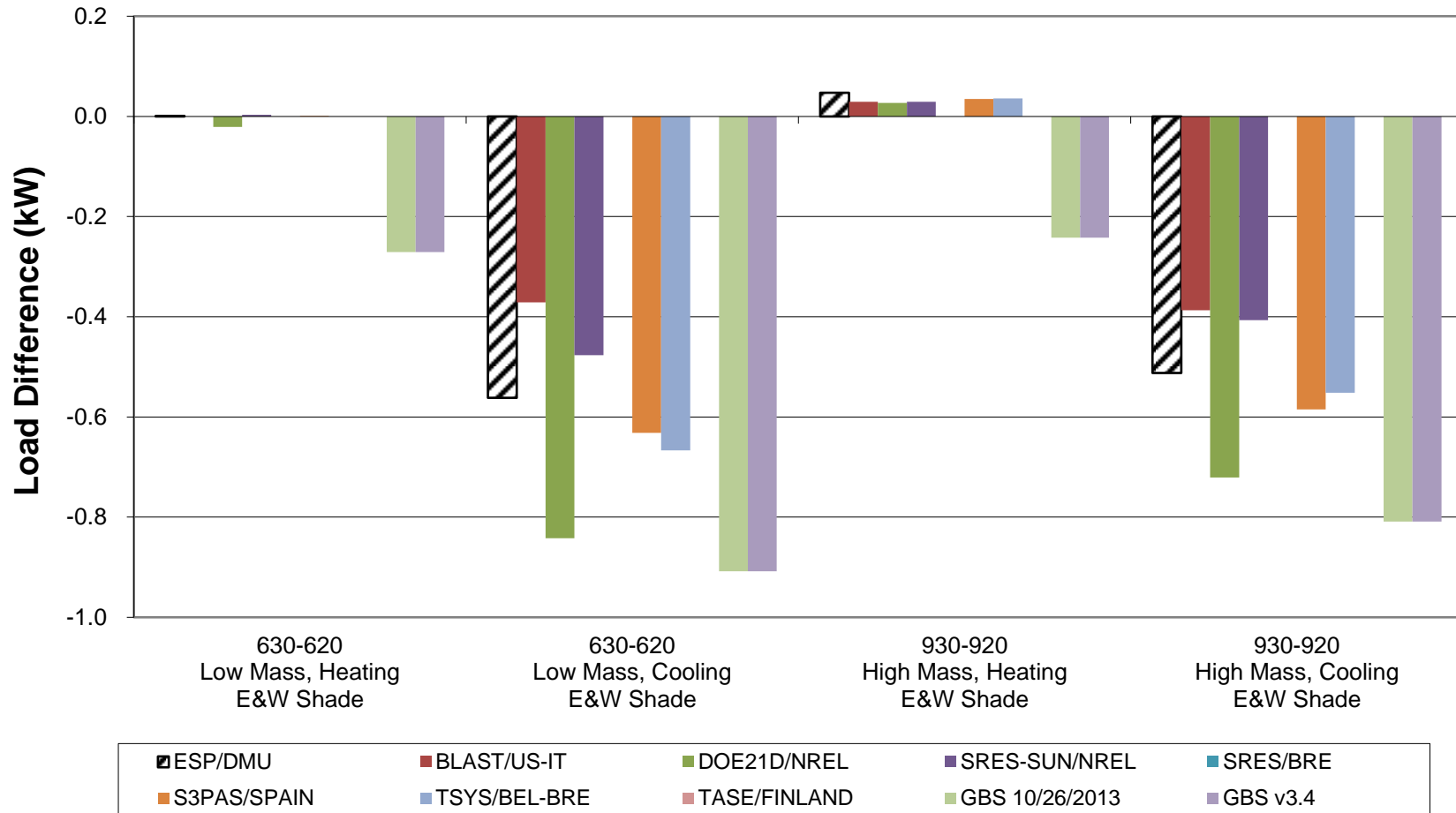
**Figure B8-20. BESTEST BASIC
 East & West Window (Delta)
 Peak Heating and Sensible Cooling**



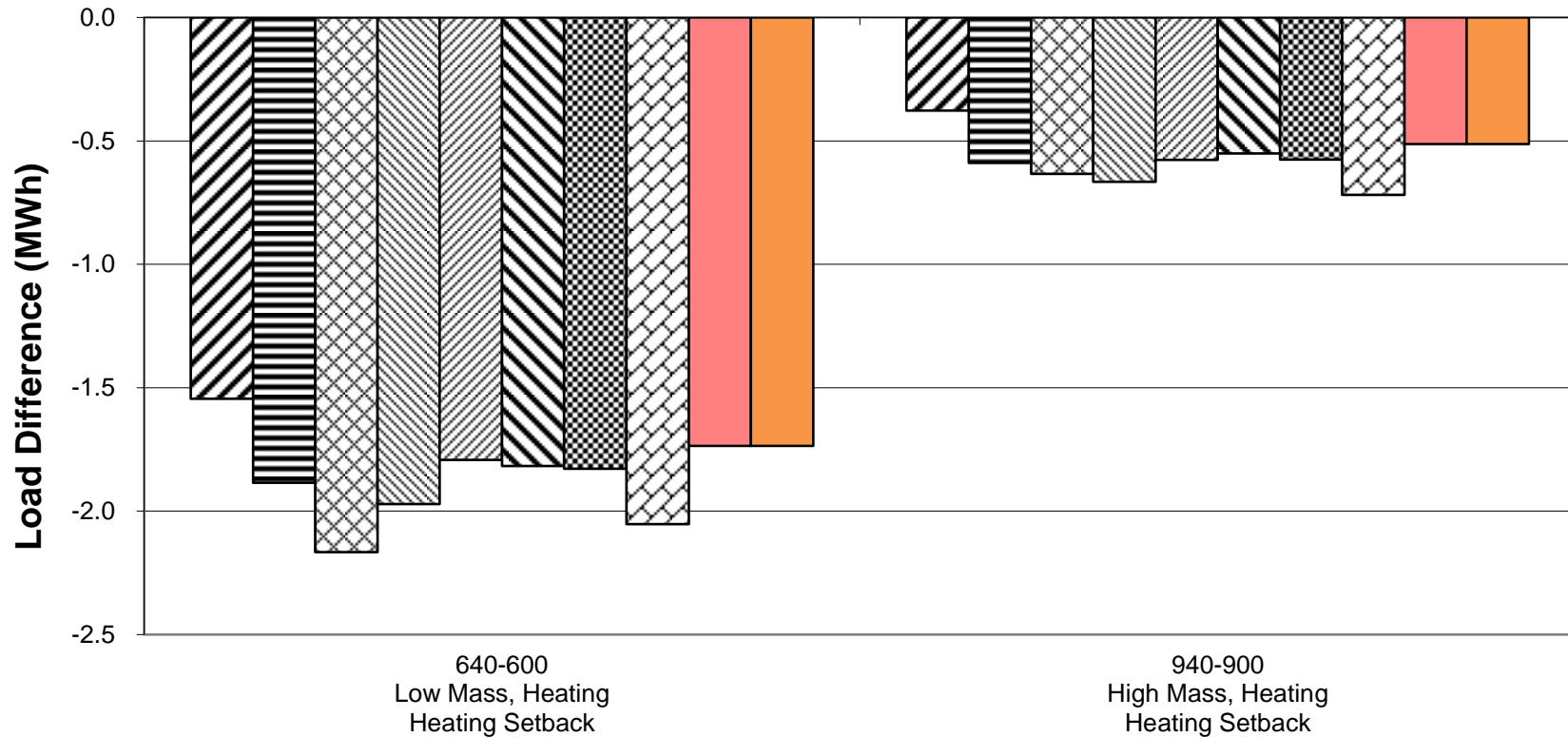
**Figure B8-21. BESTEST BASIC
 East & West Shaded Window (Delta)
 Annual Heating and Sensible Cooling**



**Figure B8-22. BESTEST BASIC
 East & West Shaded Window (Delta)
 Peak Heating and Sensible Cooling**

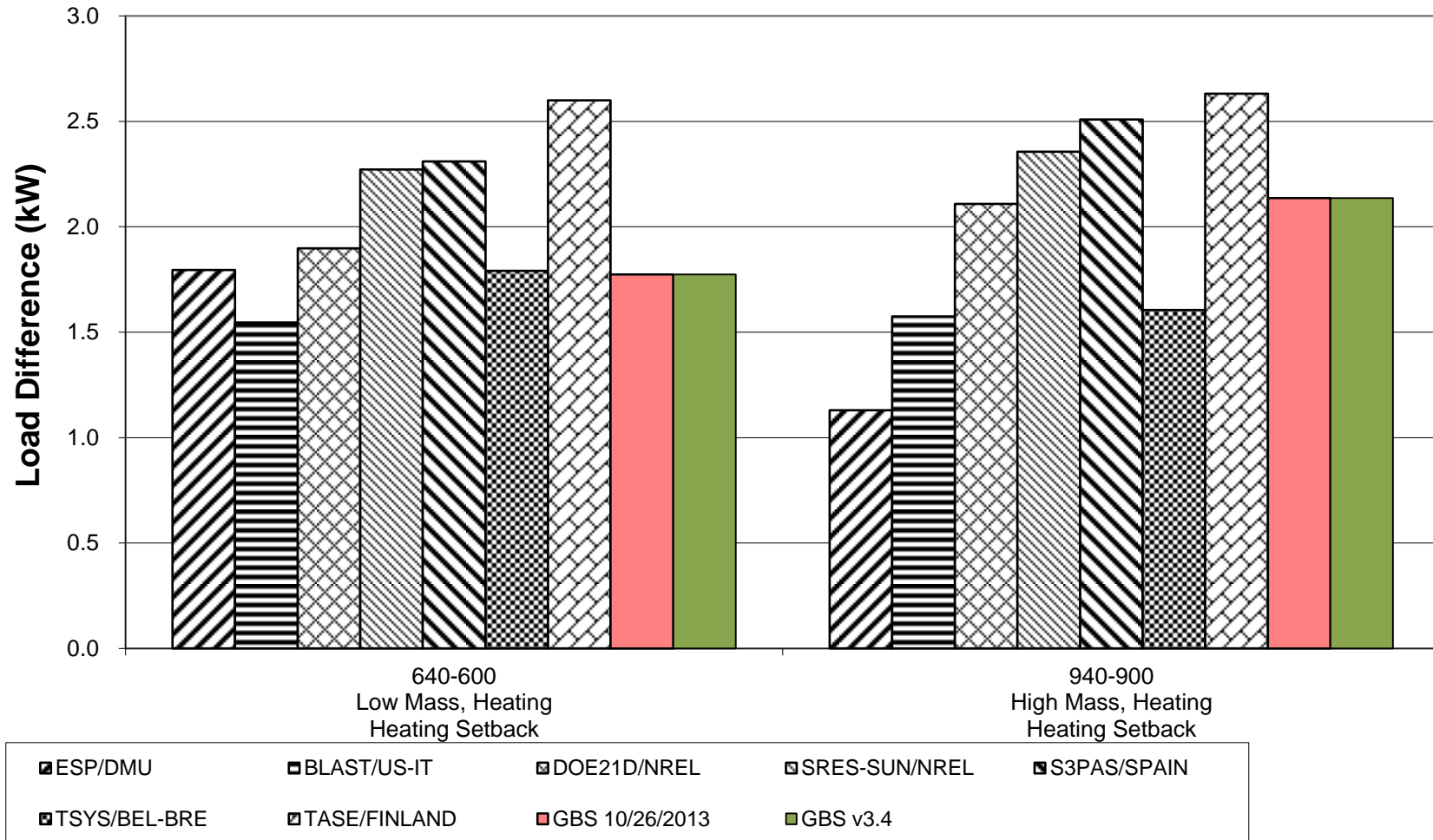


**Figure B8-23. BESTEST BASIC
 Thermostat Setback (Delta)
 Annual Heating**

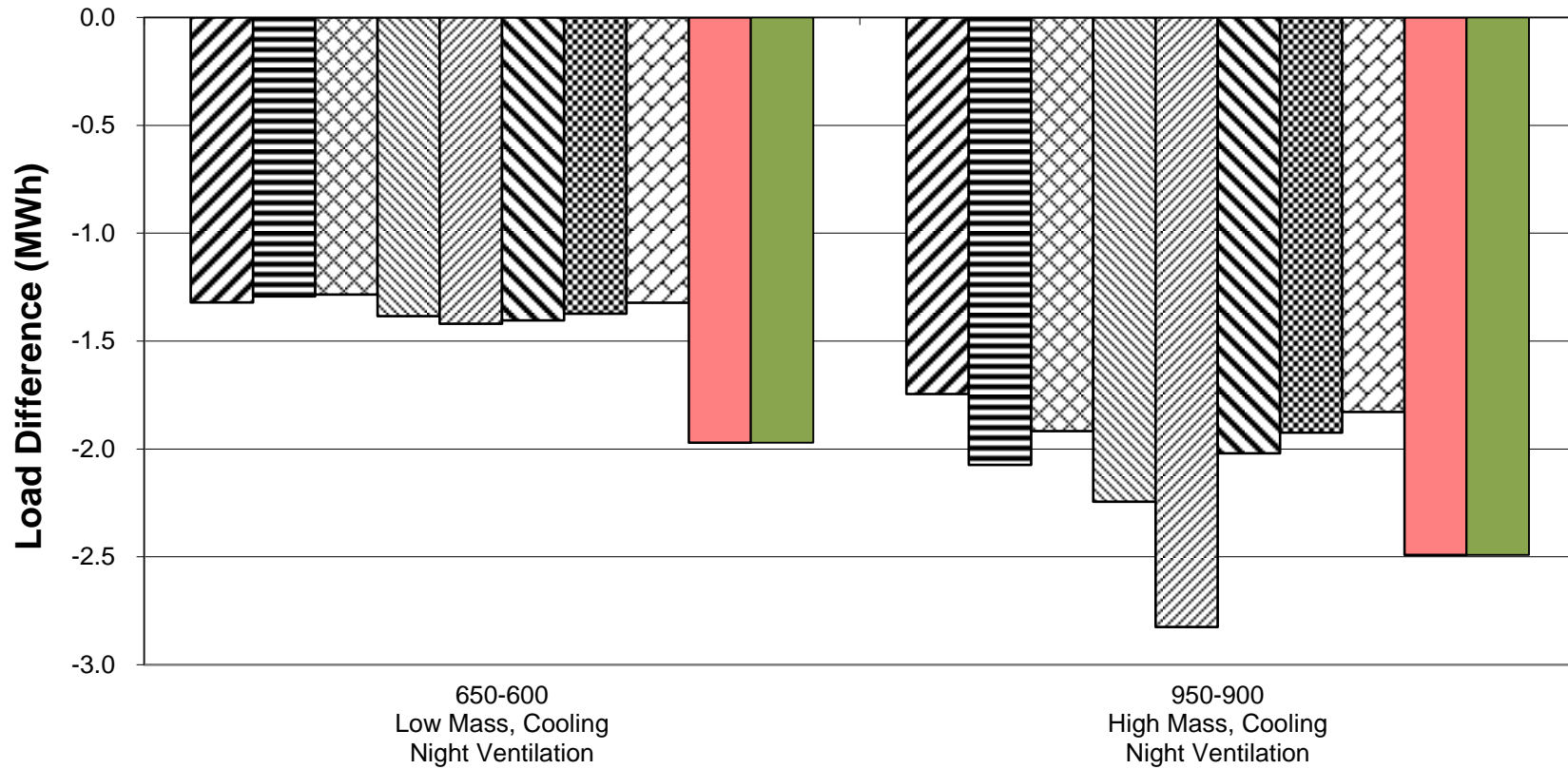


| | | | | |
|---------------|----------------|----------------|------------------|------------|
| □ ESP/DMU | ▣ BLAST/US-IT | ▣ DOE21D/NREL | ▣ SRES-SUN/NREL | ▣ SRES/BRE |
| ▣ S3PAS/SPAIN | ▣ TSYS/BEL-BRE | ▣ TASE/FINLAND | ■ GBS 10/26/2013 | ■ GBS v3.4 |

**Figure B8-24. BESTEST BASIC
 Thermostat Setback (Delta)
 Peak Heating**

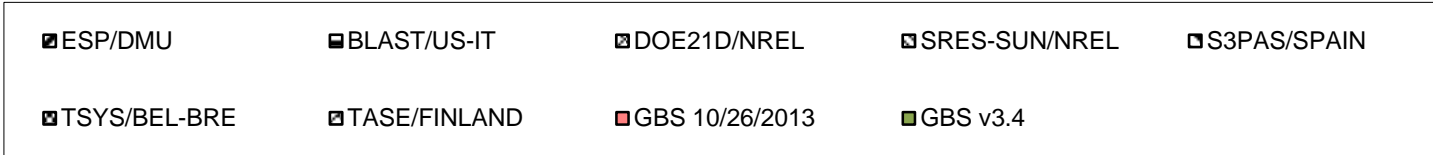
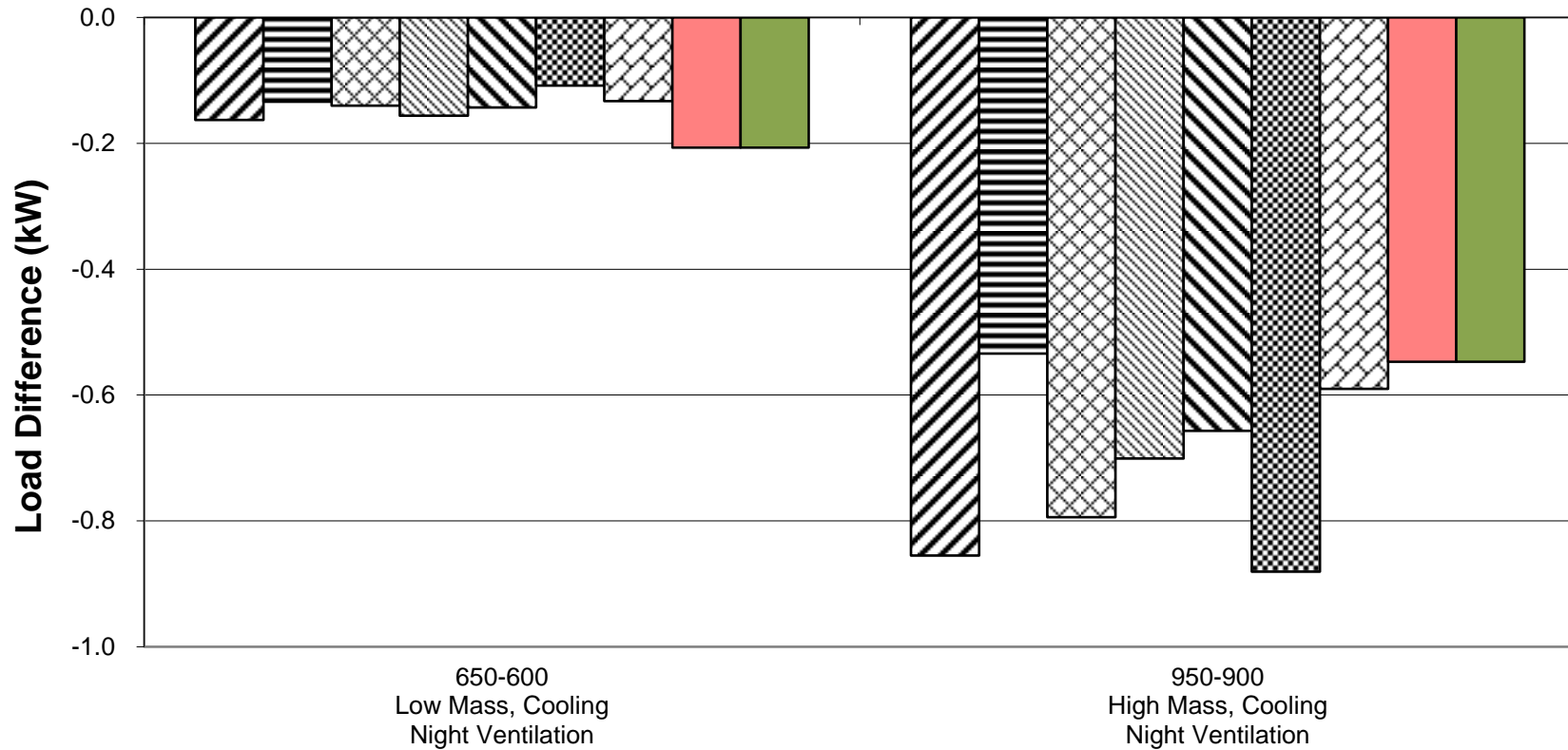


**Figure B8-25. BESTEST BASIC
 Vent Cooling (Delta)
 Annual Sensible Cooling**

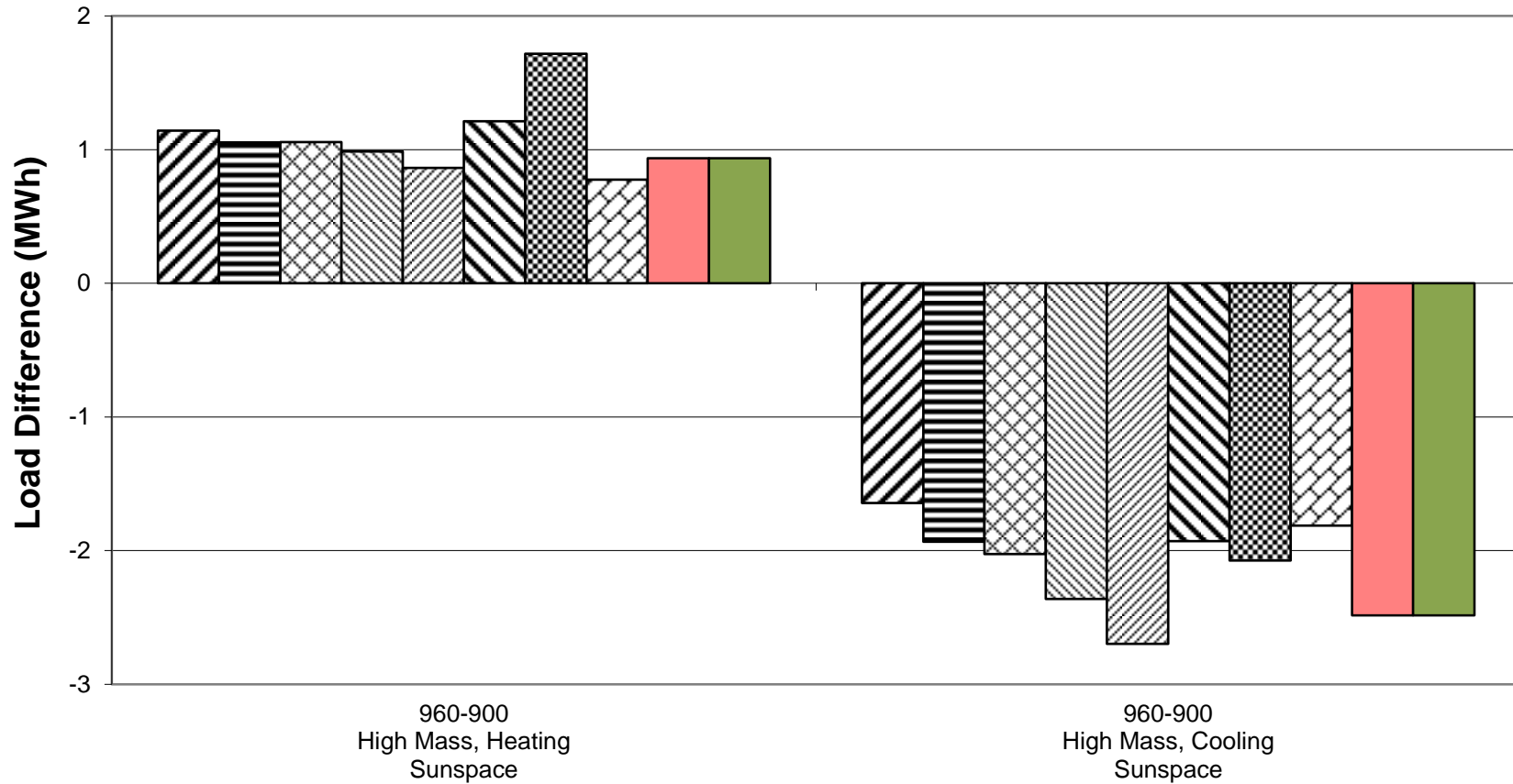


| | | | | |
|-------------|--------------|--------------|----------------|----------|
| ESP/DMU | BLAST/US-IT | DOE21D/NREL | SRES-SUN/NREL | SRES/BRE |
| S3PAS/SPAIN | TSYS/BEL-BRE | TASE/FINLAND | GBS 10/26/2013 | GBS v3.4 |

**Figure B8-26. BESTEST BASIC
 Vent Cooling (Delta)
 Peak Sensible Cooling**

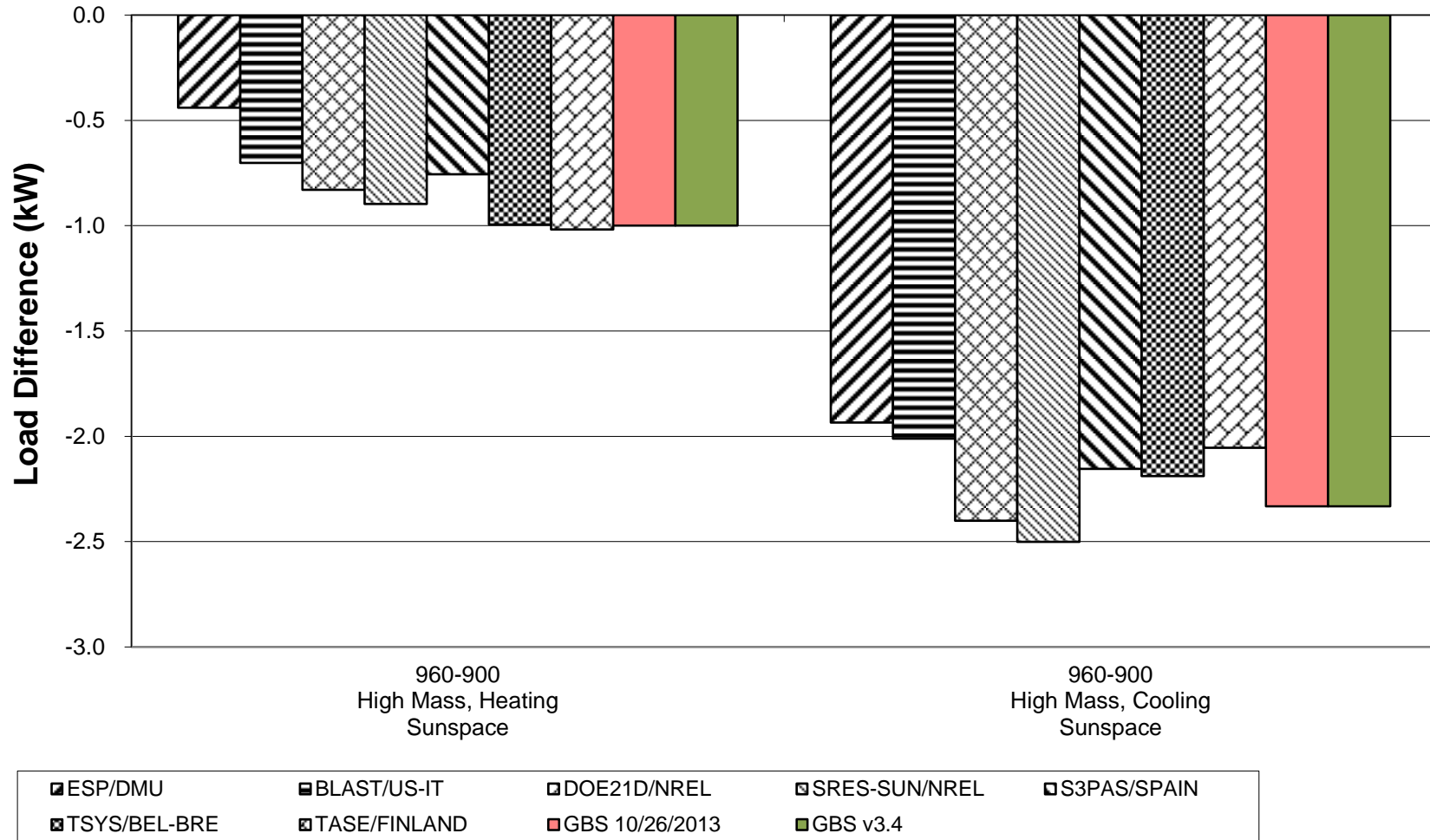


**Figure B8-27. BESTEST BASIC
 Sunspace (Delta)
 Annual Heating and Sensible Cooling**

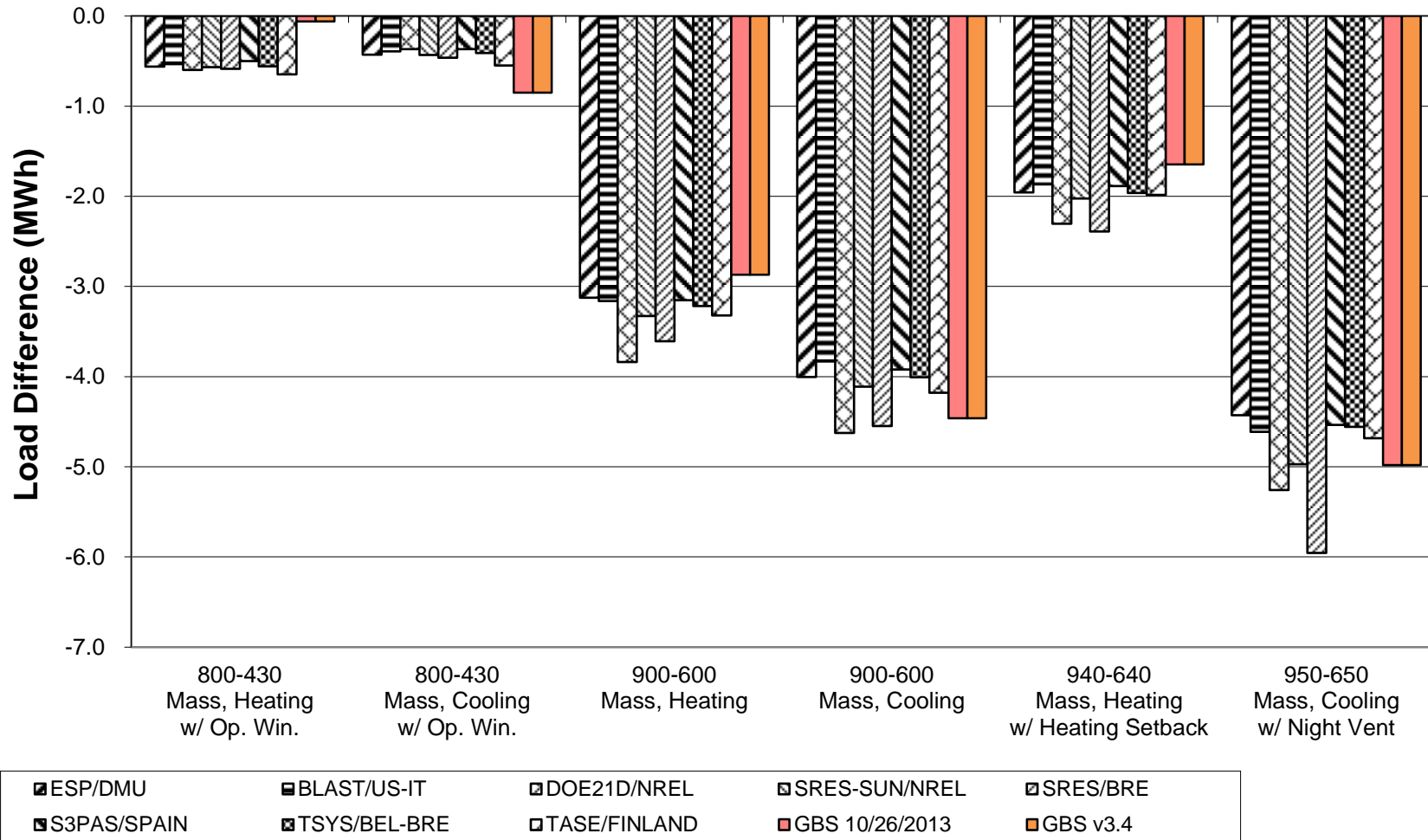


| | | | | |
|-------------|--------------|--------------|----------------|----------|
| ESP/DMU | BLAST/US-IT | DOE21D/NREL | SRES-SUN/NREL | SRES/BRE |
| S3PAS/SPAIN | TSYS/BEL-BRE | TASE/FINLAND | GBS 10/26/2013 | GBS v3.4 |

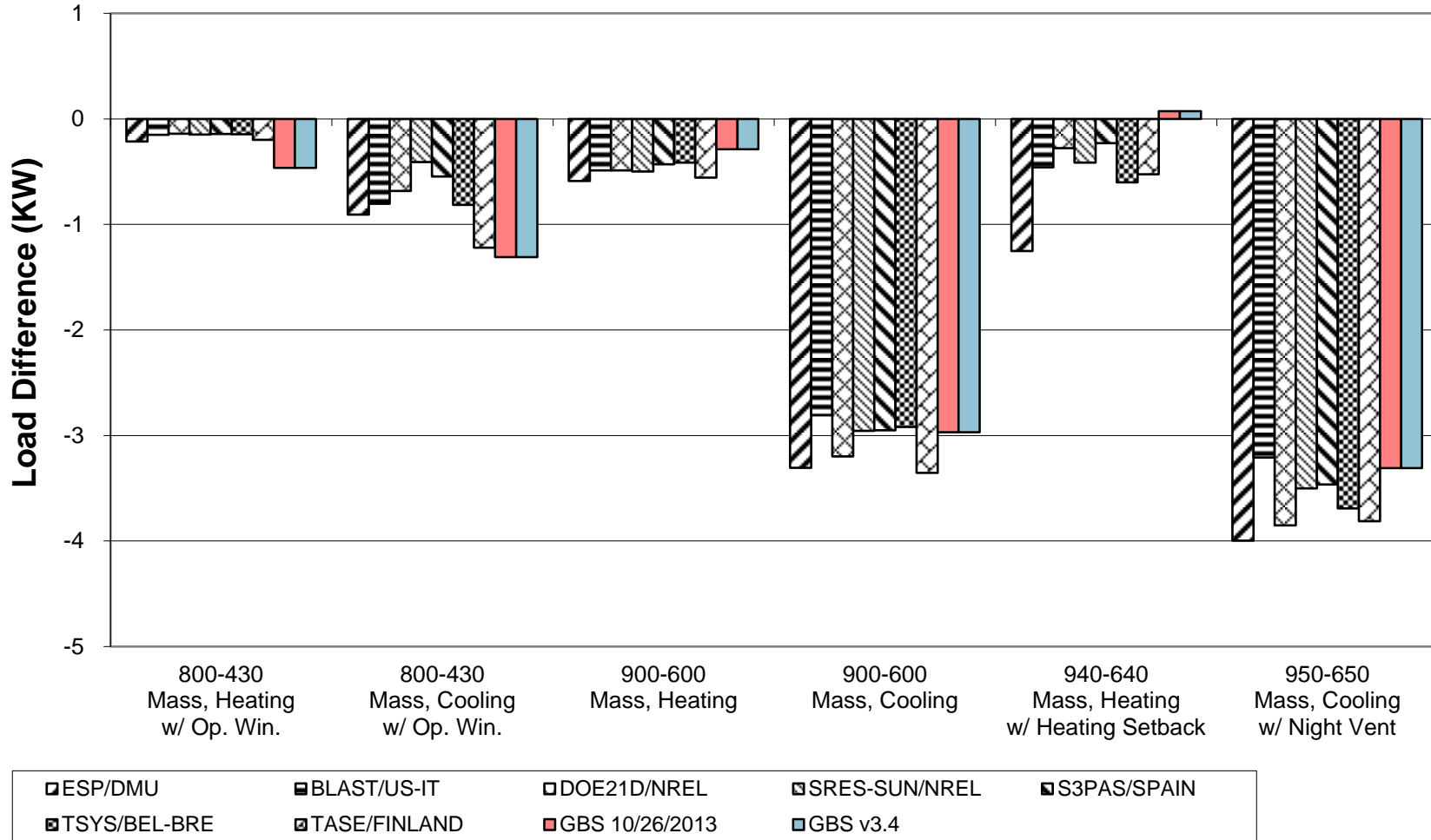
**Figure B8-28. BESTEST BASIC
 Sunspace (Delta)
 Peak Heating and Sensible Cooling**



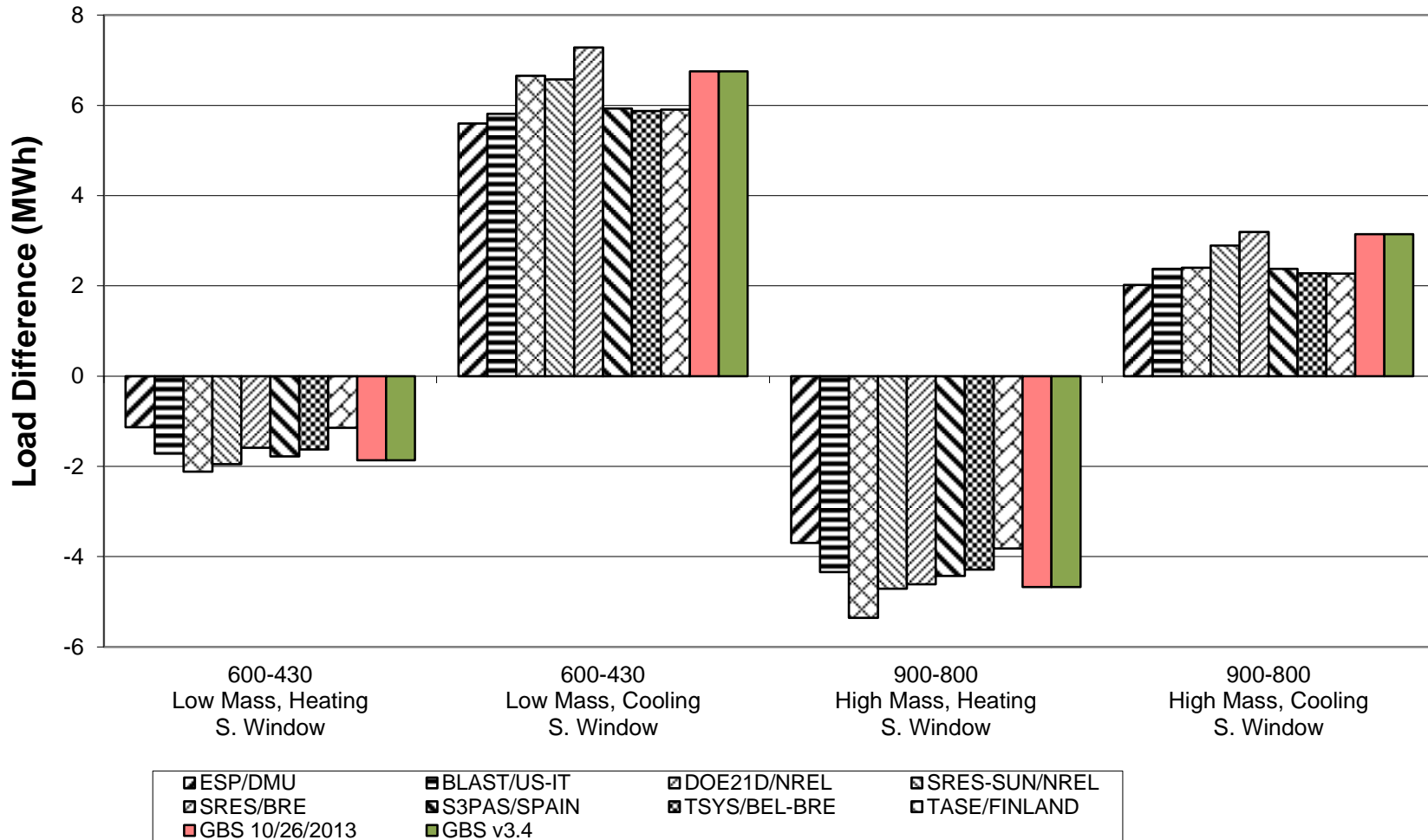
**Figure B8-29. BESTEST BASIC AND IN-DEPTH
 Mass Effect (Delta)
 Annual Heating and Sensible Cooling**



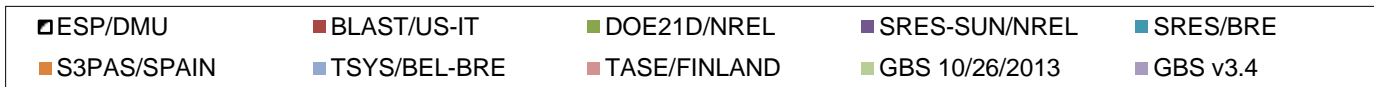
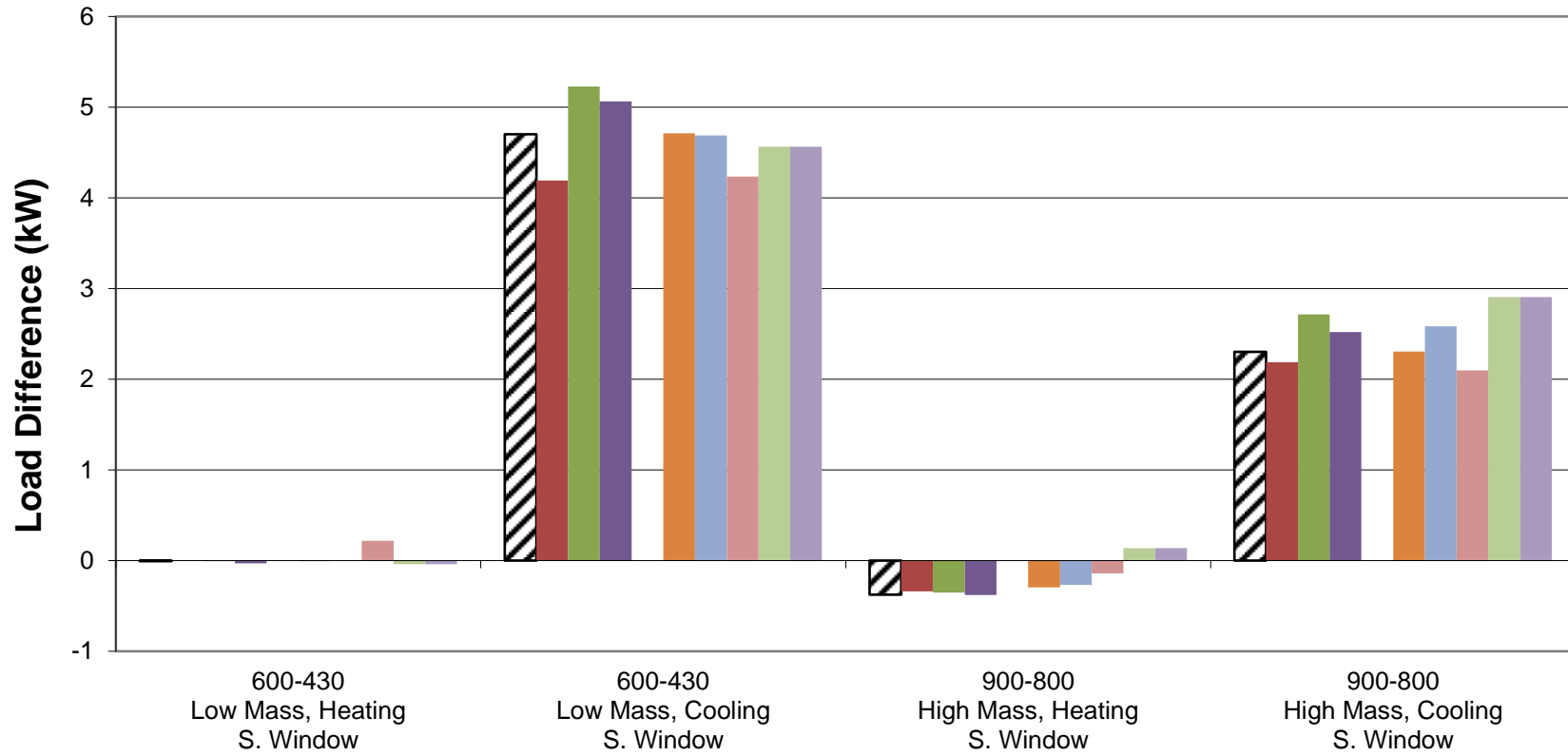
**Figure B8-30. BESTEST BASIC AND IN-DEPTH
 Mass Effect (Delta)
 Peak Heating and Sensible Cooling**



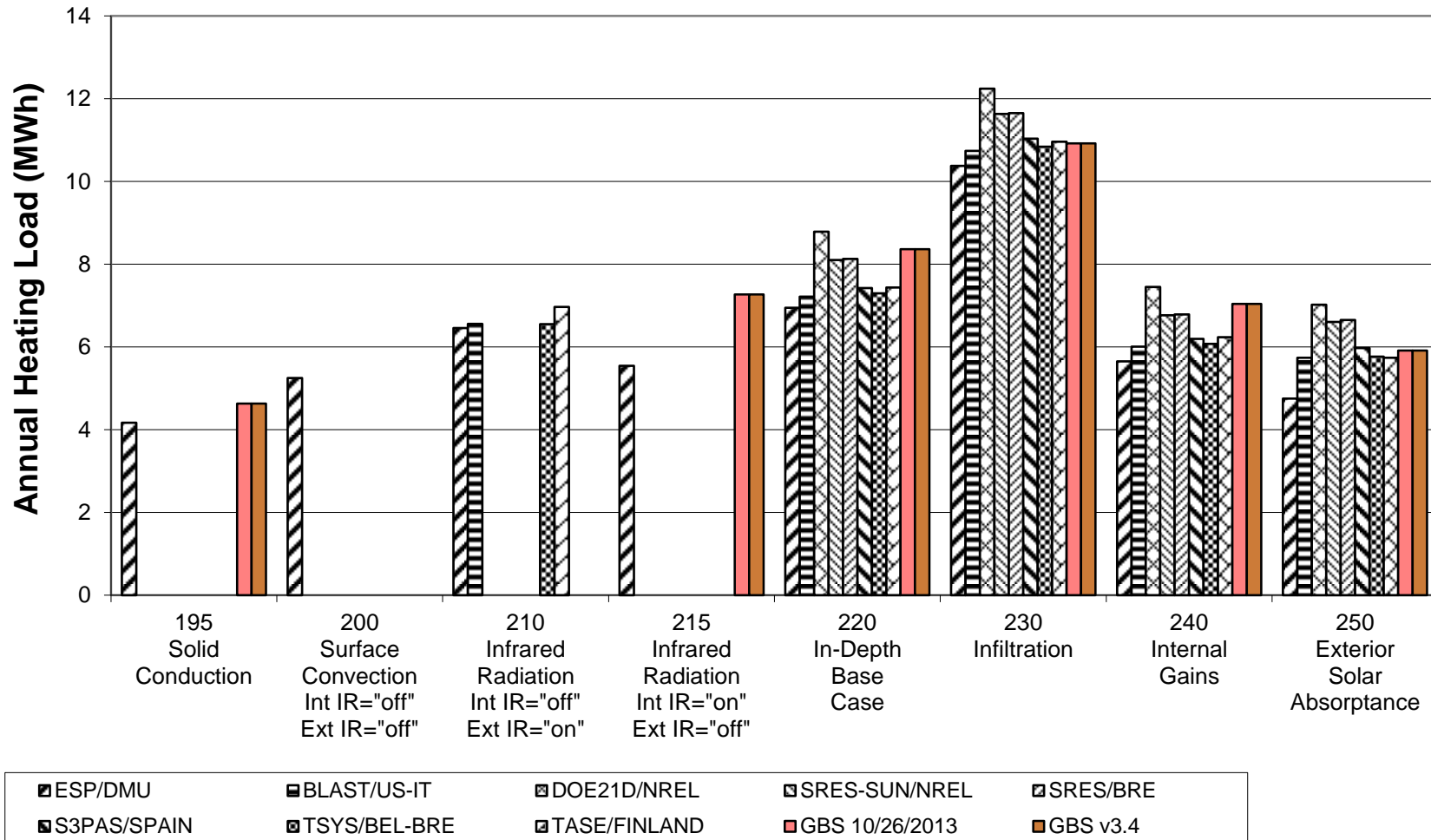
**Figure B8-31. BESTEST IN-DEPTH
 South Window (Delta)
 Annual Heating and Sensible Cooling**



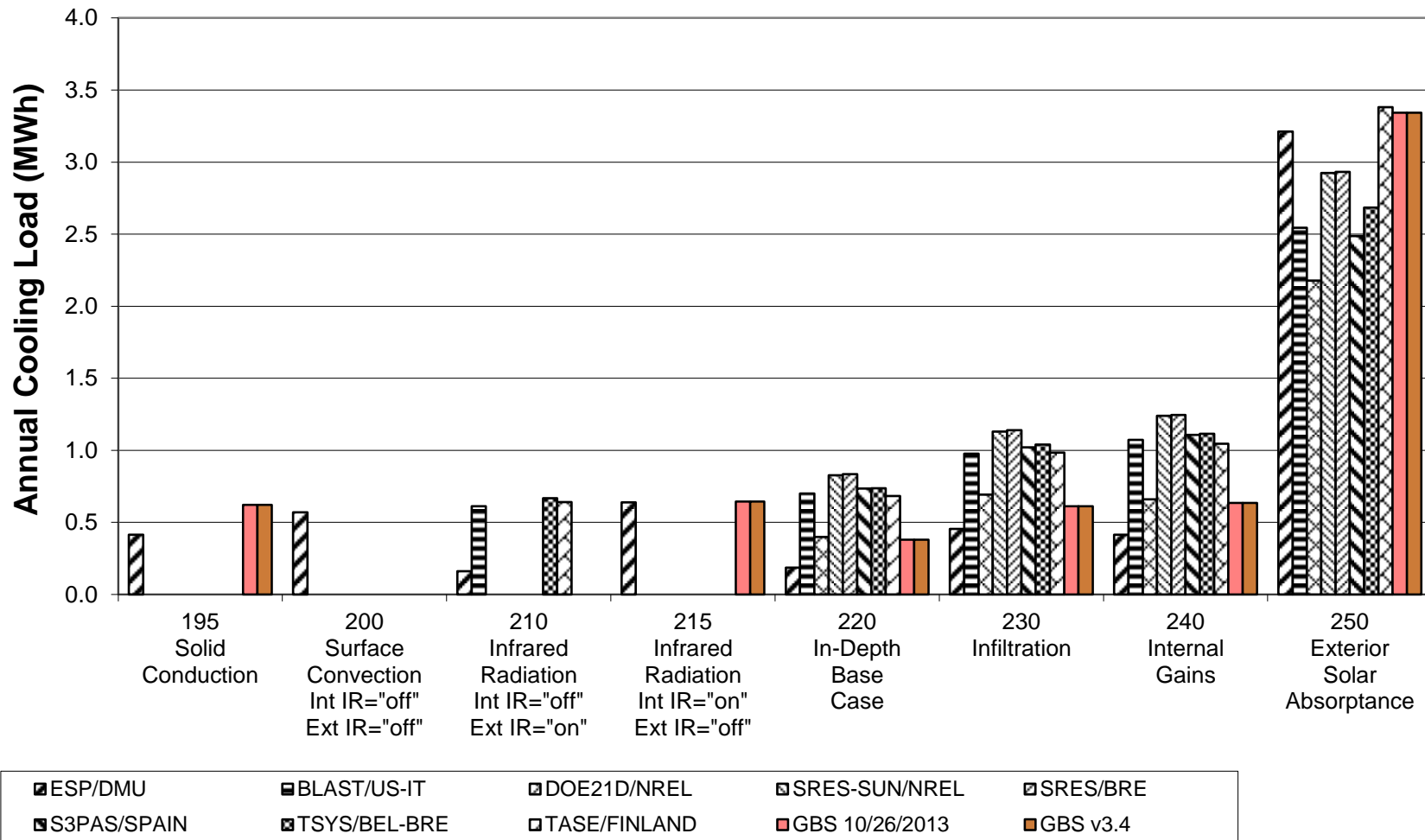
**Figure B8-32. BESTEST IN-DEPTH
 South Window (Delta)
 Peak Heating and Sensible Cooling**



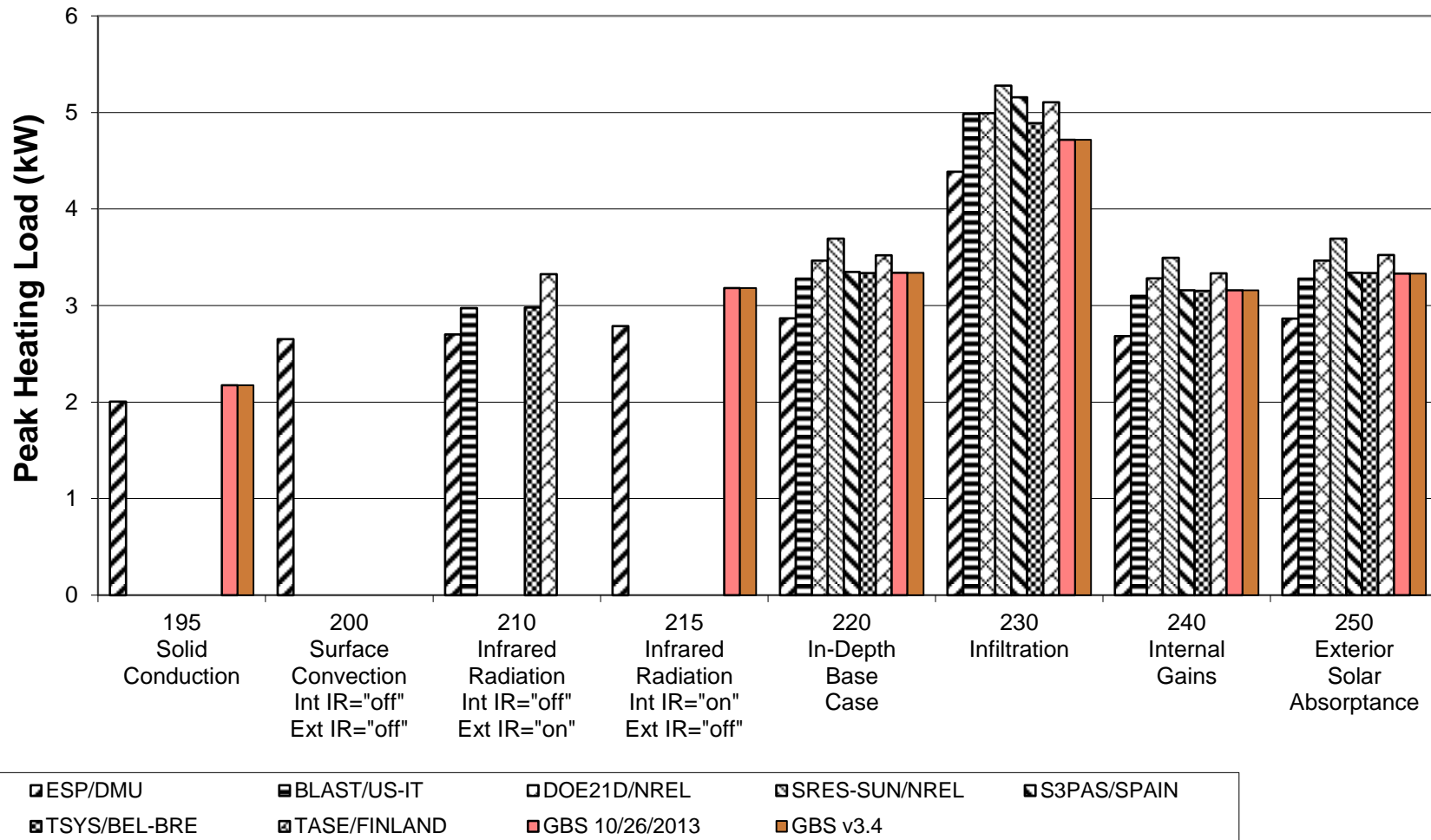
**Figure B8-33. BESTEST IN-DEPTH
 Low Mass Annual Heating
 Cases 195 to 250**



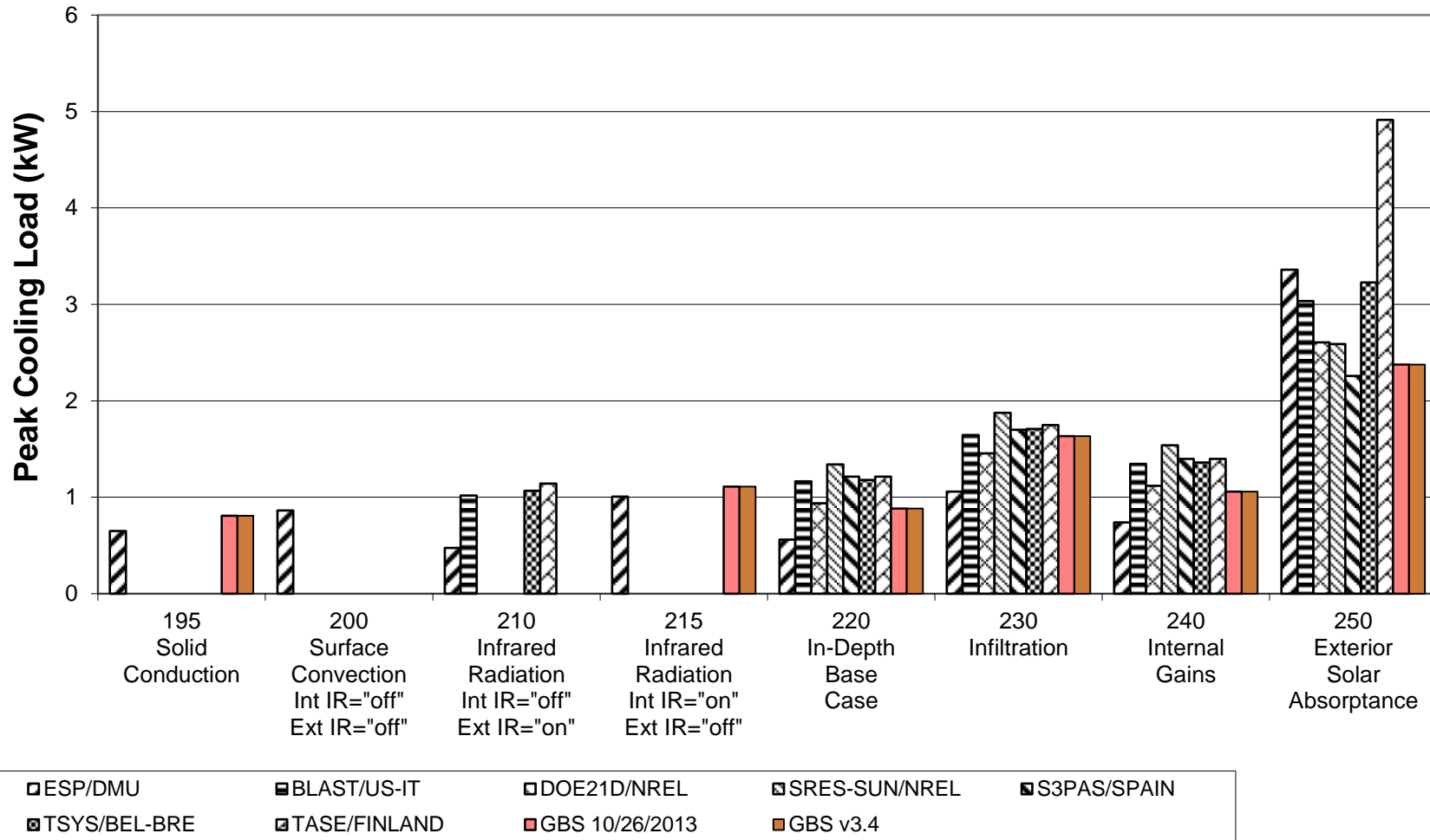
**Figure B8-34. BESTEST IN-DEPTH
 Low Mass Annual Sensible Cooling
 Cases 195 to 250**



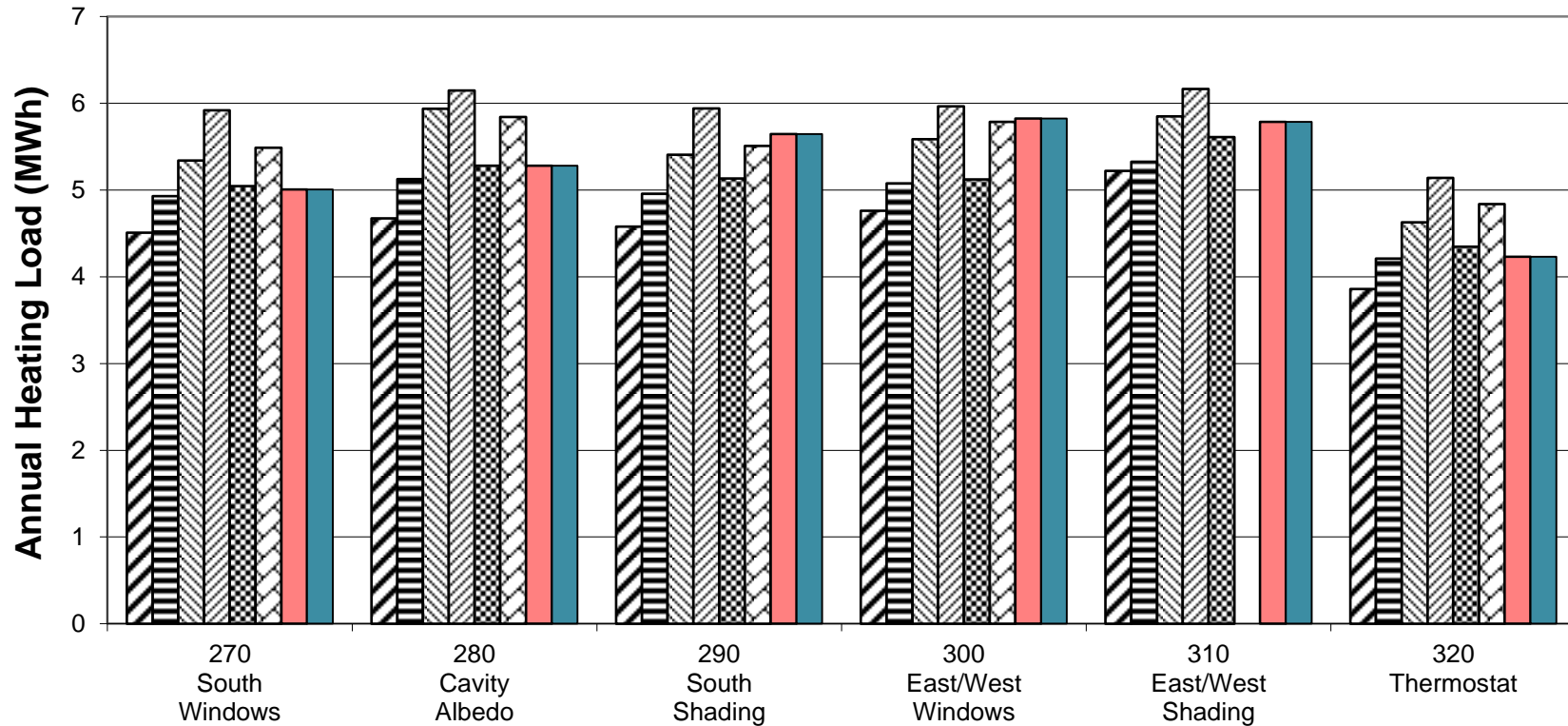
**Figure B8-35. BESTEST IN-DEPTH
 Low Mass Peak Heating
 Cases 195 to 250**



**Figure B8-36. BESTEST IN-DEPTH
 Low Mass Peak Sensible Cooling
 Cases 195 to 250**



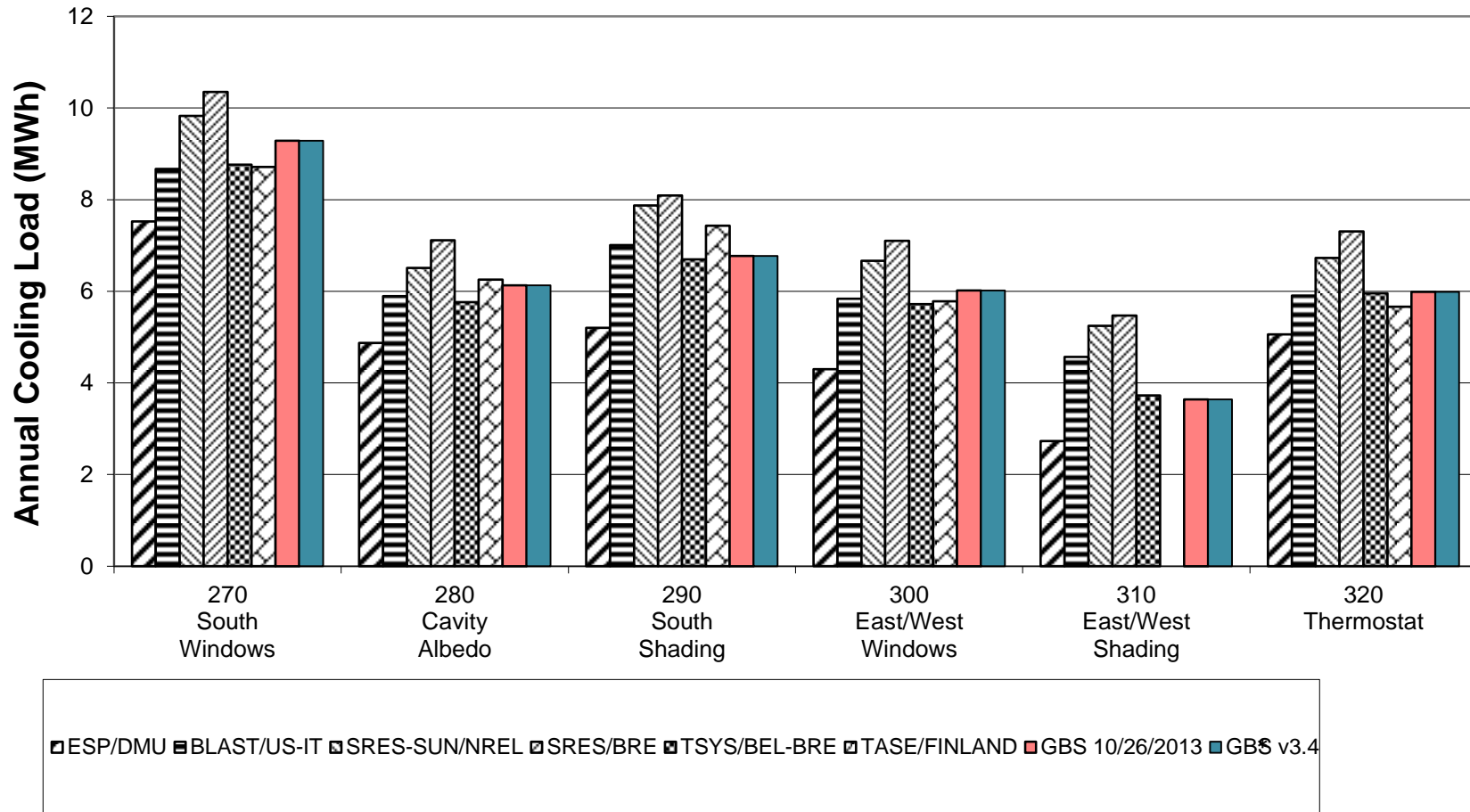
**Figure B8-37. BESTEST IN-DEPTH
Low Mass Annual Heating
Cases 270 to 320**



ESP/DMU
 BLAST/US-IT
 SRES-SUN/NREL
 SRES/BRE
 TSYB/BEL-BRE
 TASE/FINLAND
 GBS 10/26/2013
 GBS v3.4*

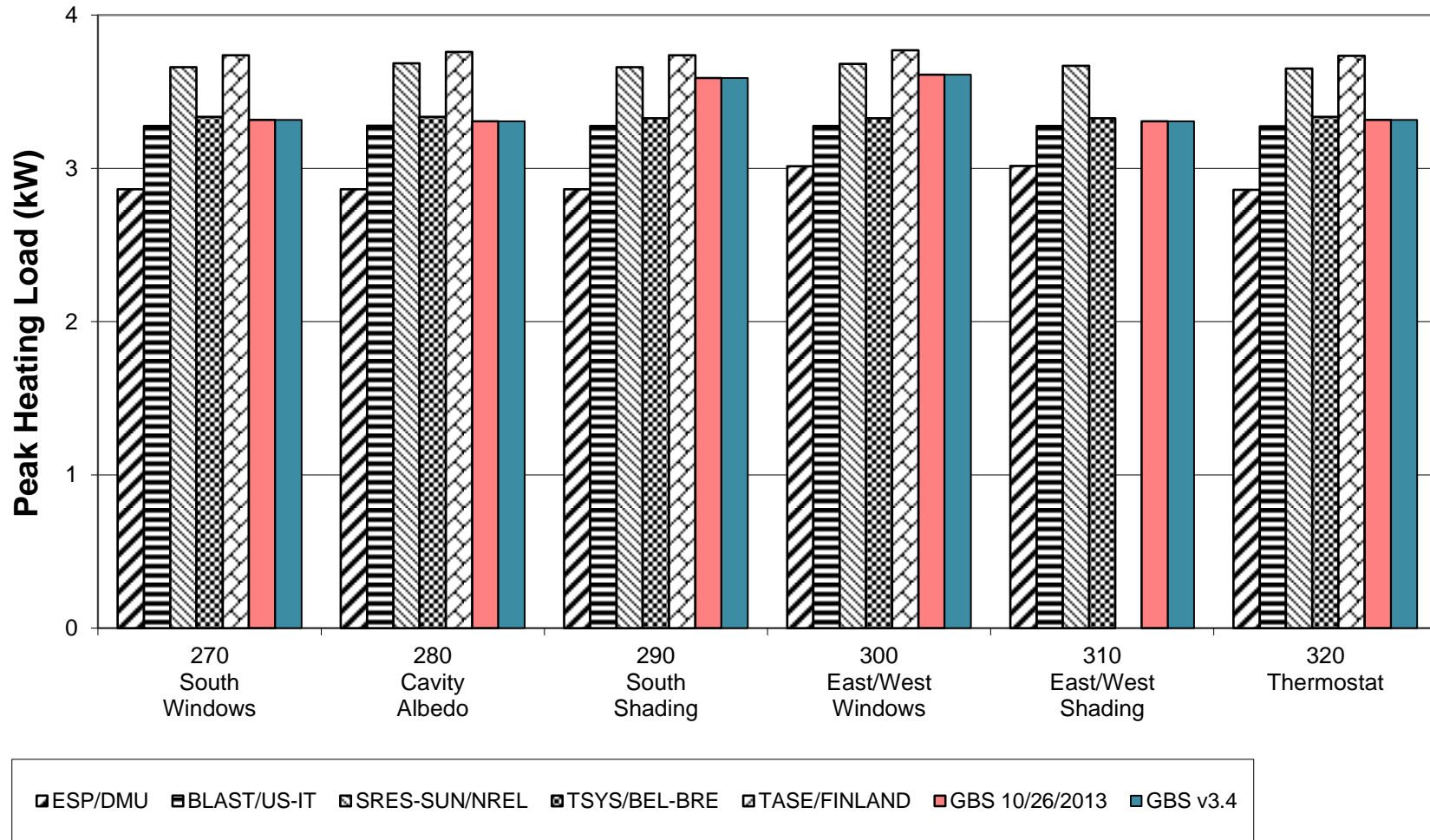
* SRES/BRE Cases 270, 290-320 have input error likely affecting results by <0.2 MWh/y (<3%)

**Figure B8-38. BESTEST IN-DEPTH
 Low Mass Annual Sensible Cooling
 Cases 270 to 320**

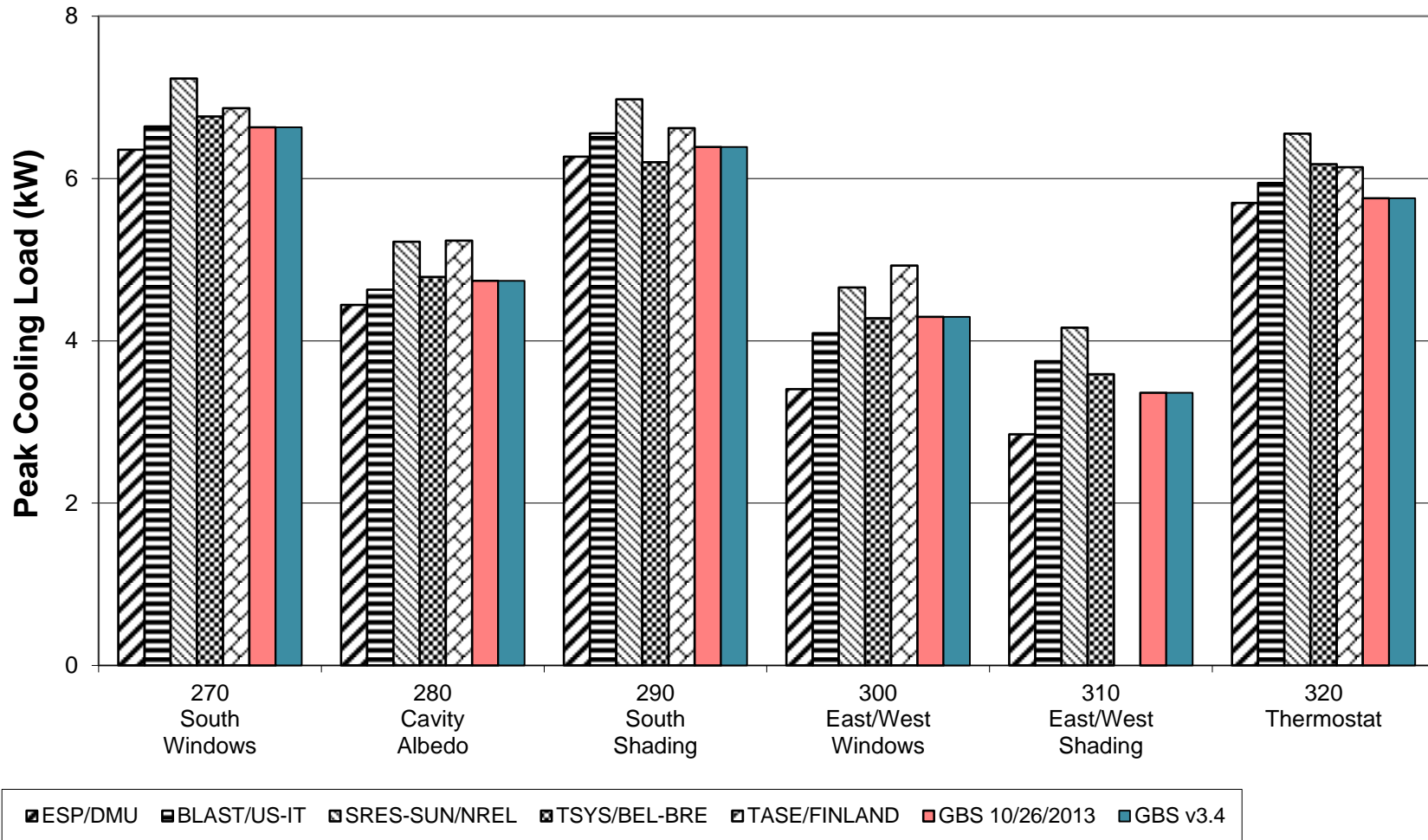


* SRES/BRE Cases 270, 290-320 have input error likely affecting results by <0.2 MWh/y (<3%)

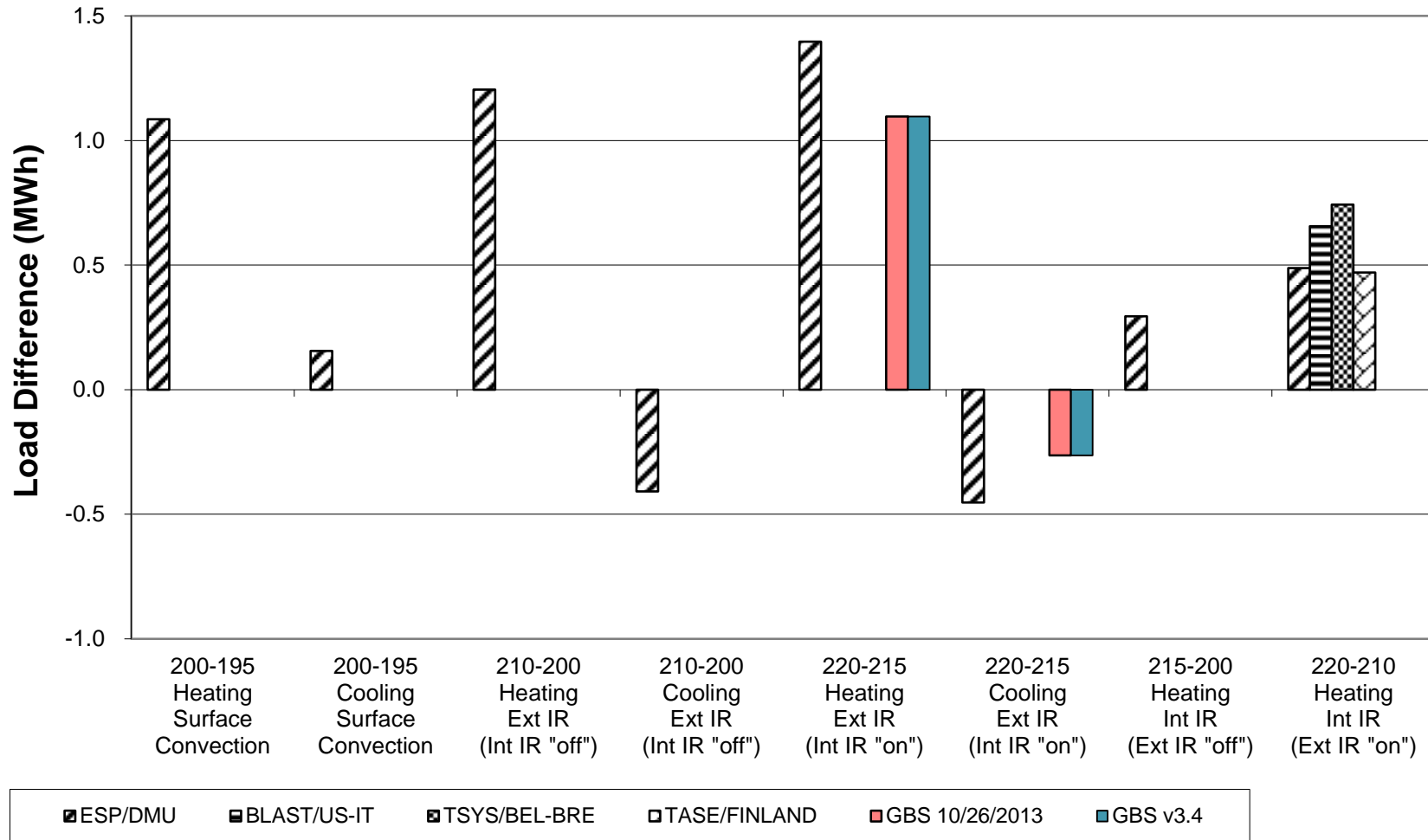
**Figure B8-39. BESTEST IN-DEPTH
 Low Mass Peak Heating
 Cases 270 to 320**



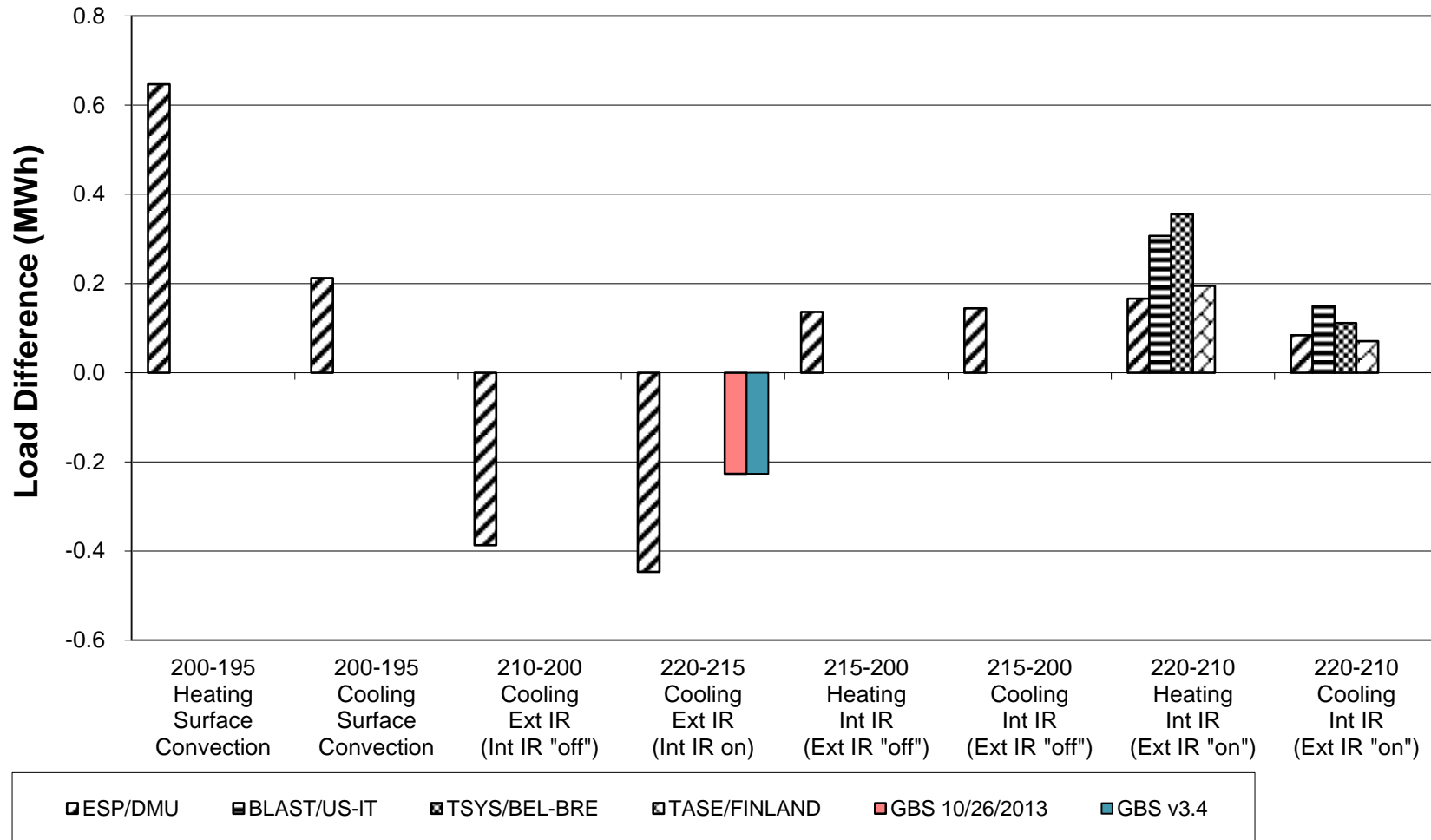
**Figure B8-40. BESTEST IN-DEPTH
 Low Mass Peak Sensible Cooling
 Cases 270 to 320**



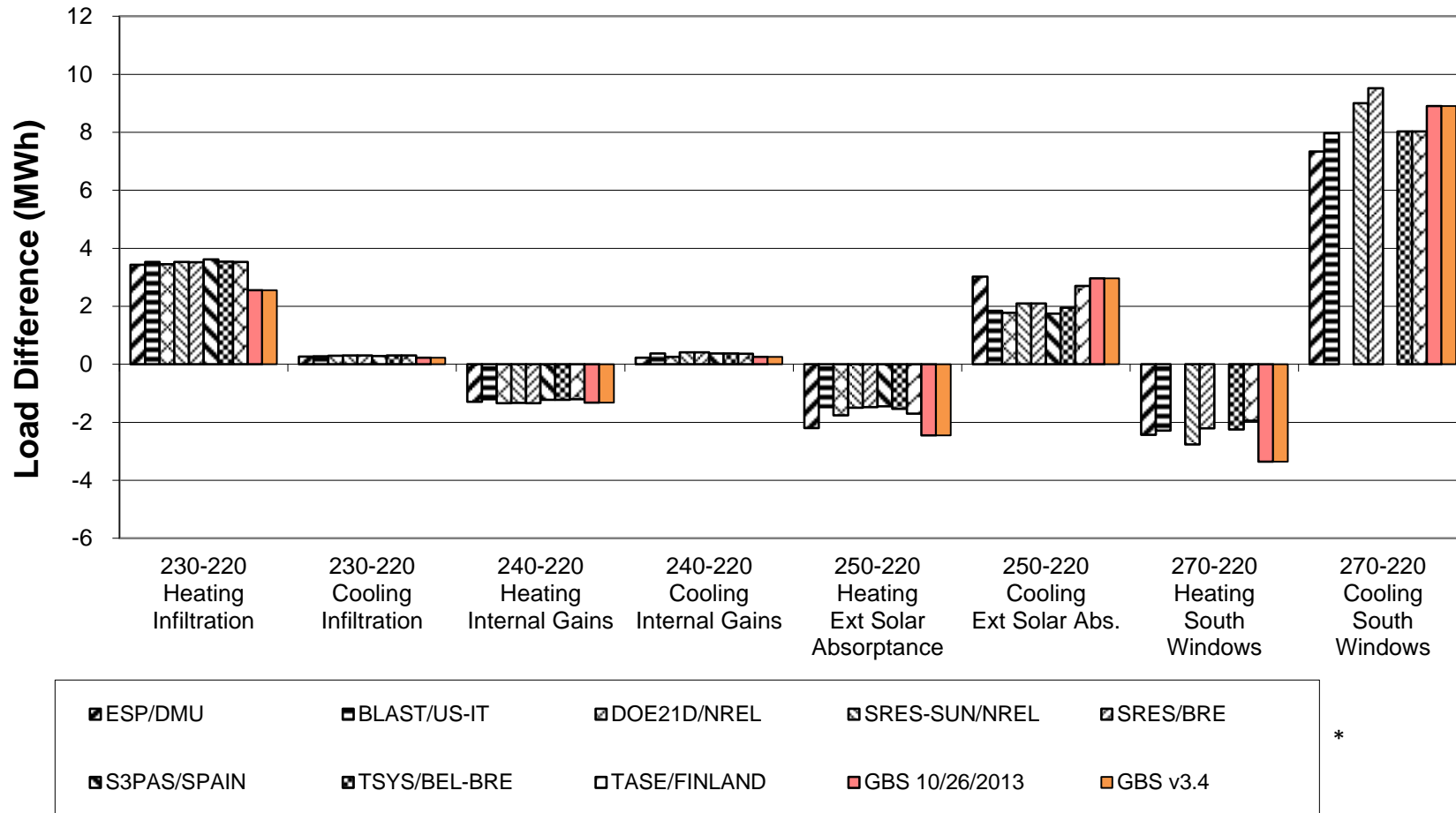
**Figure B8-41. BESTEST IN-DEPTH
 Cases 195 to 220 (Delta)
 Annual Heating and Sensible Cooling**



**Figure B8-42. BESTEST IN-DEPTH
Cases 195 to 220 (Delta)
Peak Heating and Sensible Cooling**

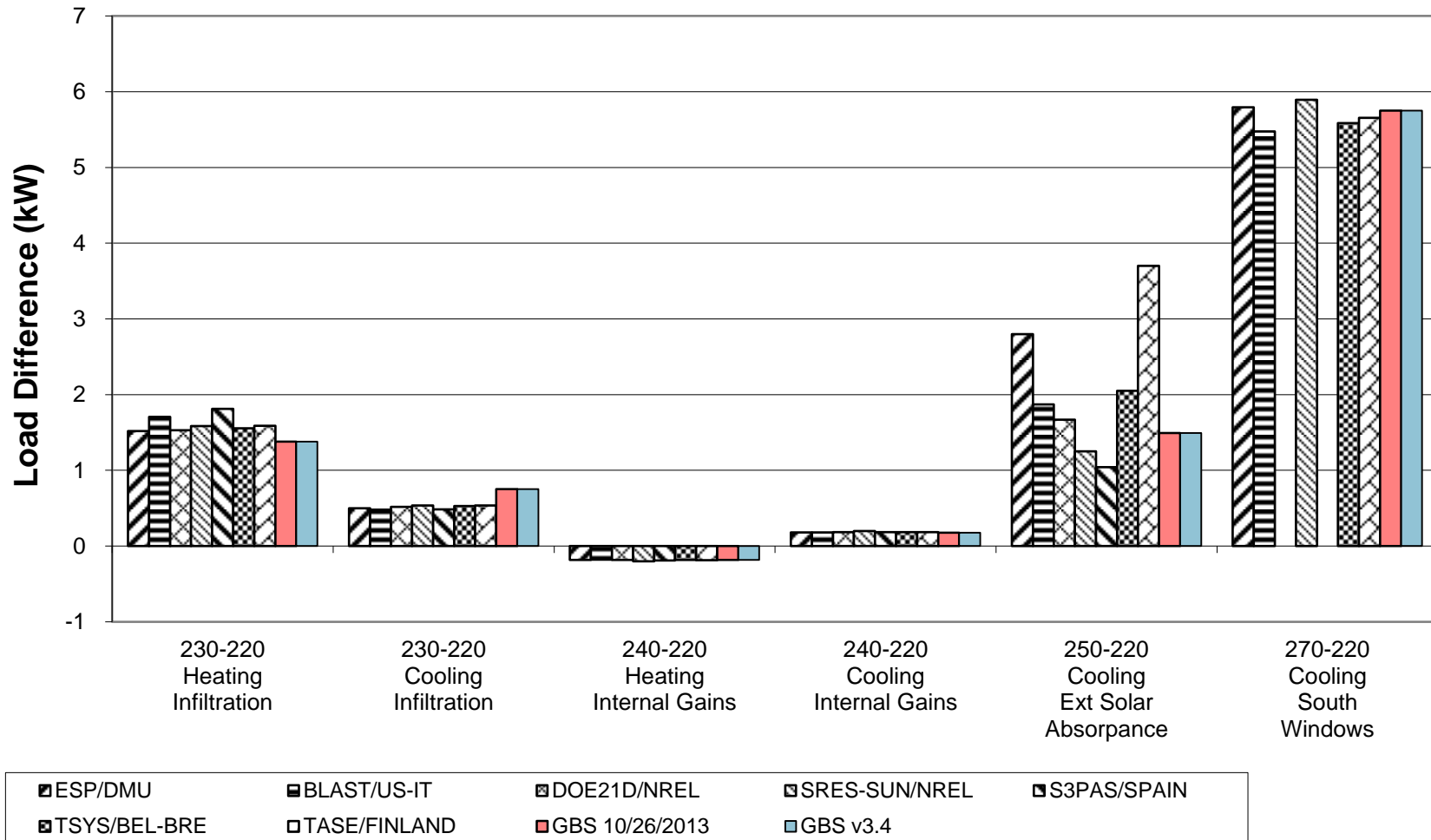


**Figure B8-43. BESTEST IN-DEPTH
Cases 220 to 270 (Delta)
Annual Heating and Sensible Cooling**

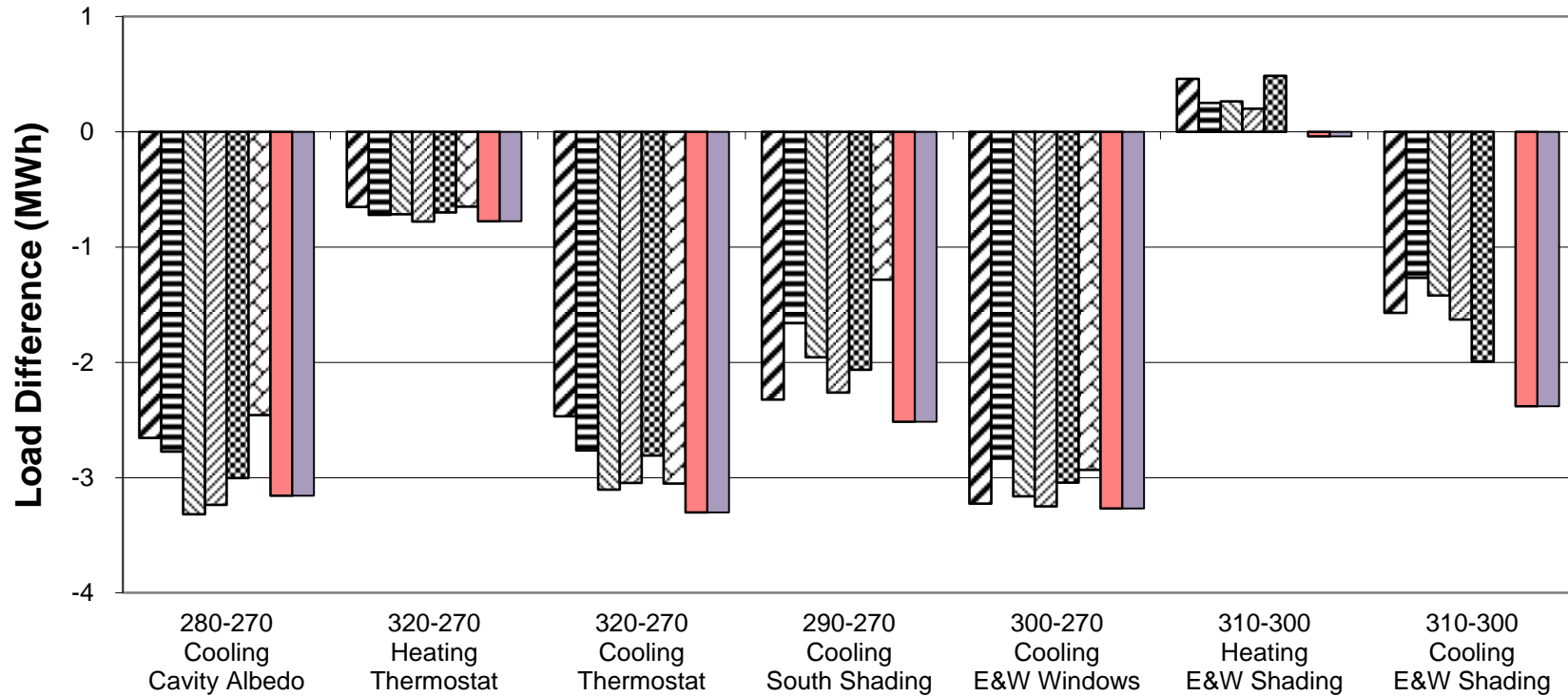


* SRES/BRE Case 270 has input error likely affecting 270-220 sensitivity results for heating by <0.2 MWh/y (<6%), and for cooling by <0.2 MWh/y (<3%)

**Figure B8-44. BESTEST IN-DEPTH
 Cases 220 to 270 (Delta)
 Peak Heating and Sensible Cooling**



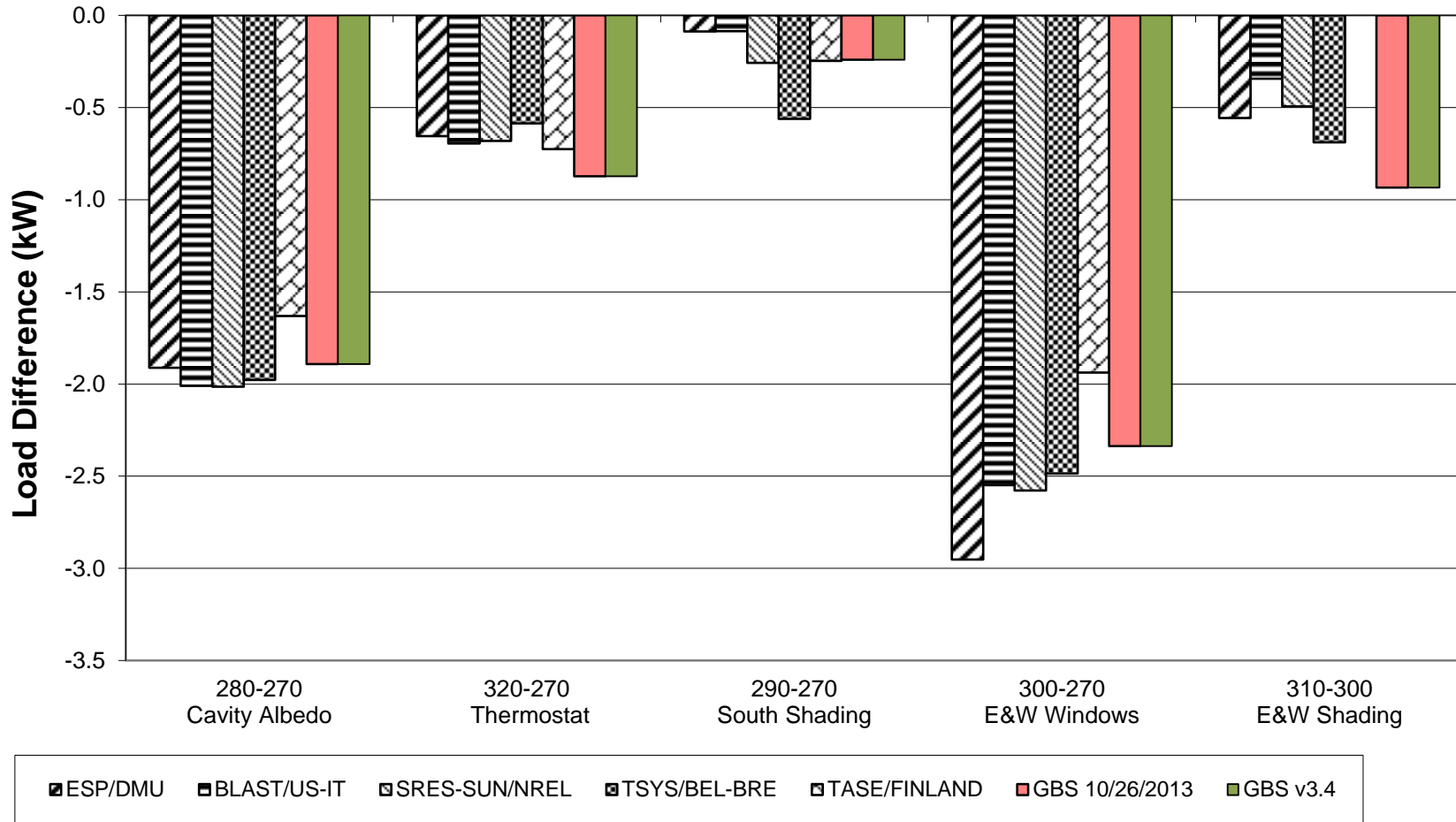
**Figure B8-45. BESTEST IN-DEPTH
 Cases 270 to 320 (Delta)
 Annual Heating and Sensible Cooling**



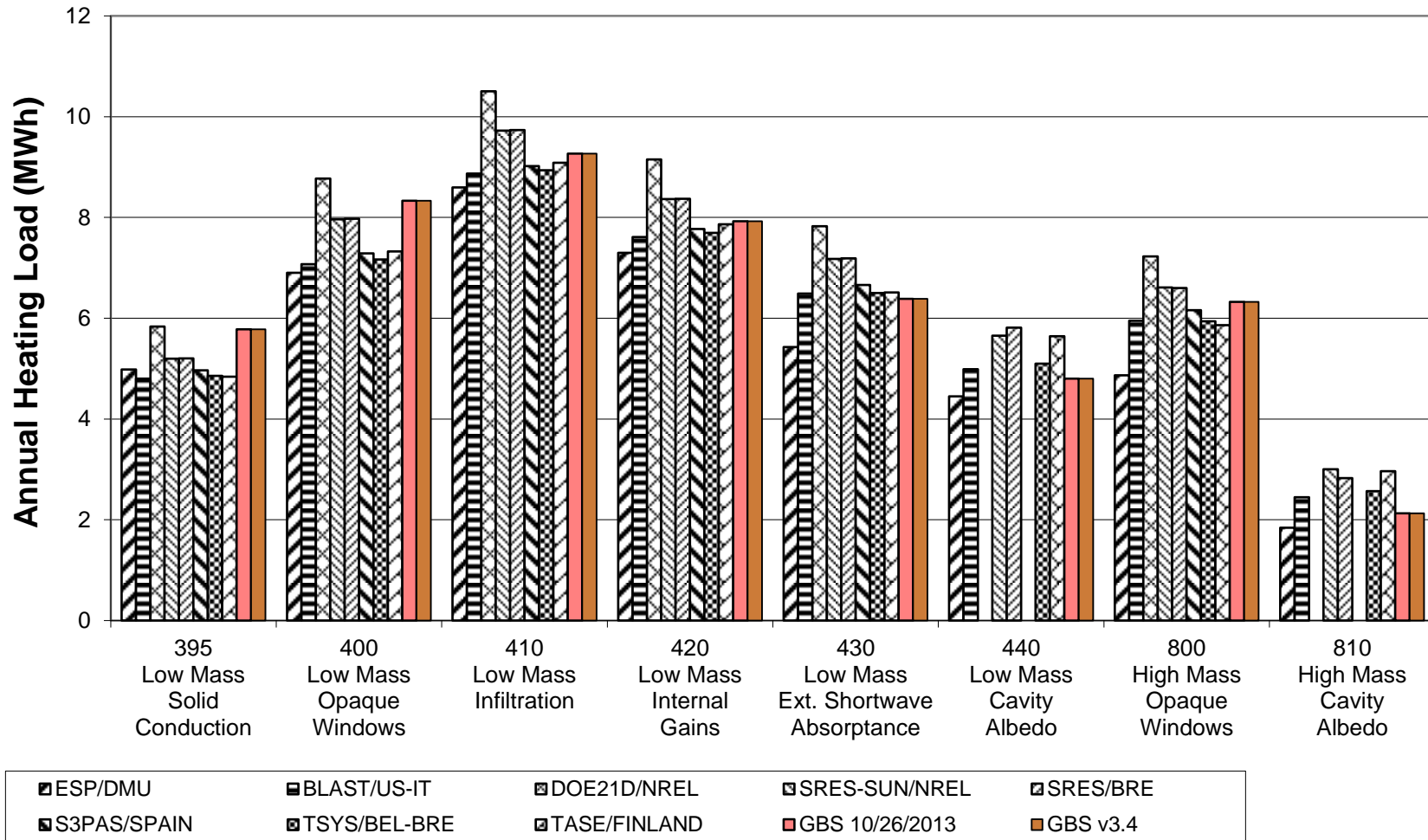
■ ESP/DMU
 ■ BLAST/US-IT
 ■ SRES-SUN/NREL
 ■ SRES/BRE
 ■ TSYS/BEL-BRE
 ■ TASE/FINLAND
 ■ GBS 10/26/2013
 ■ GBS v3.4

* SRES-BRE Cases 270, 290-320 have input error likely affecting sensitivity results for heating by <math><0.2 \text{ MWh/y}</math> (<math><6\%</math>), and for cooling by <math><0.2 \text{ MWh/y}</math> (<math><3\%</math>)

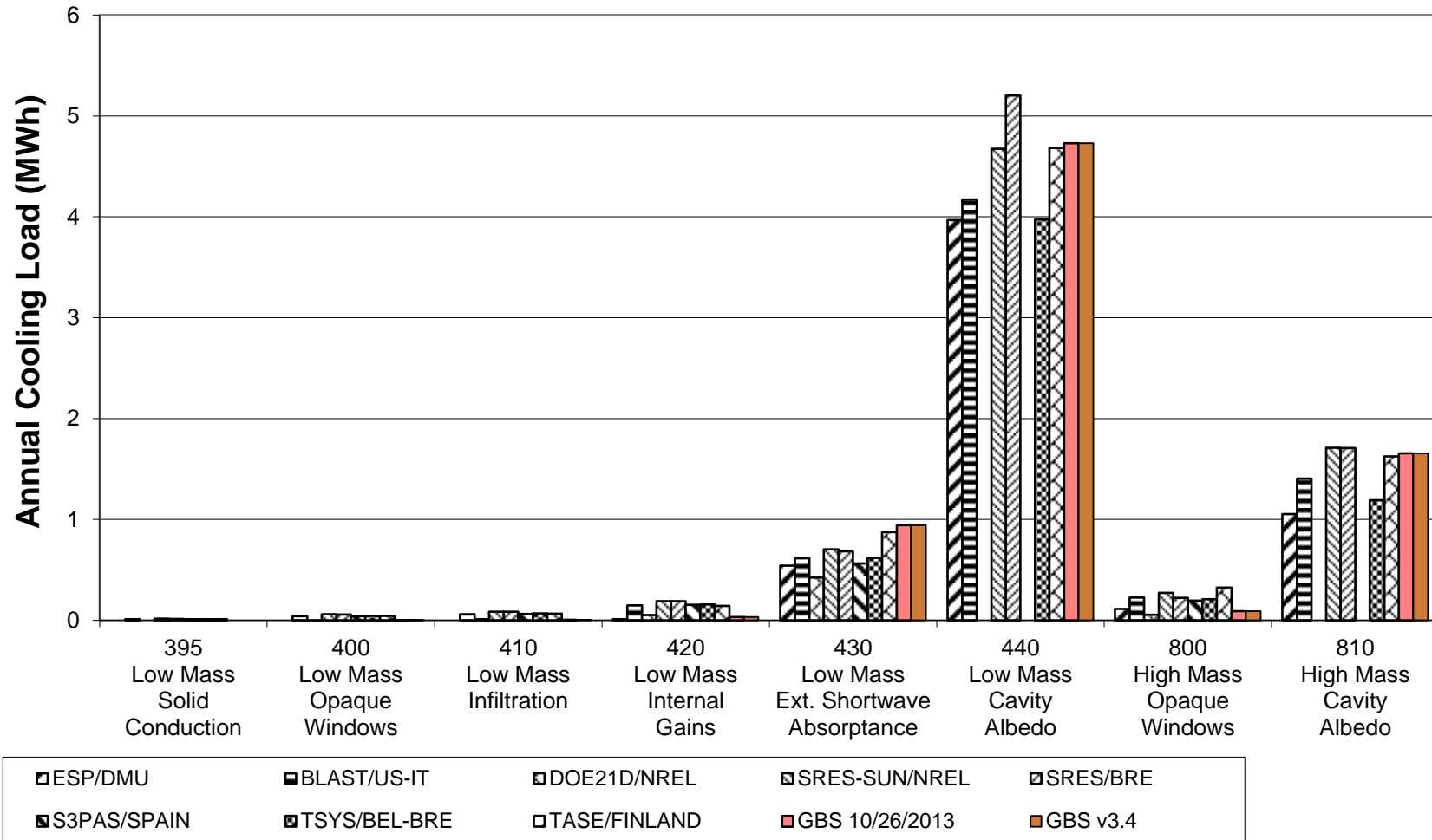
**Figure B8-46. BESTEST IN-DEPTH
 Cases 270 to 320 (Delta)
 Peak Sensible Cooling**



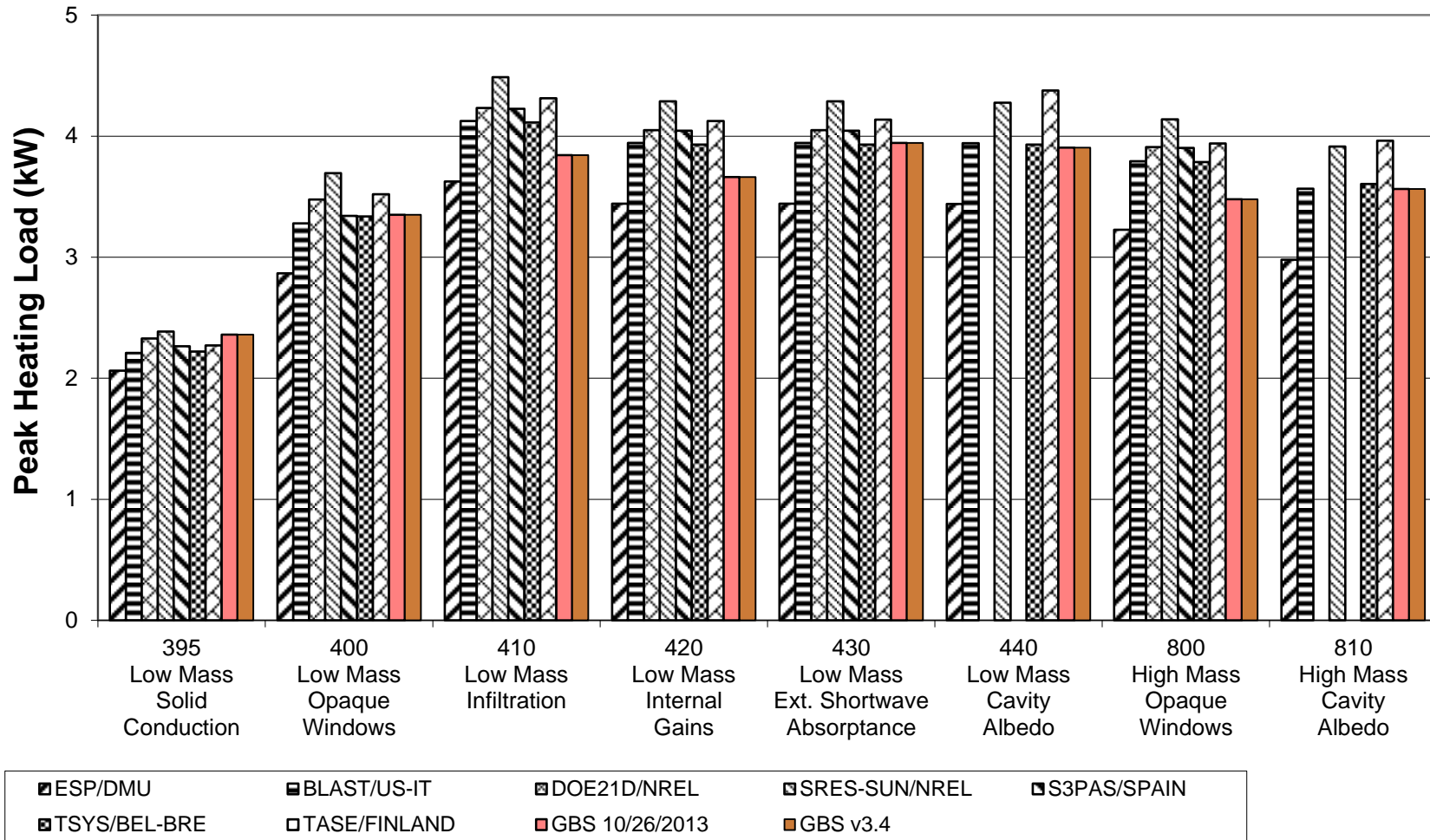
**Figure B8-47. BESTEST IN-DEPTH
 Annual Heating
 Cases 395 to 440, 800, 810**



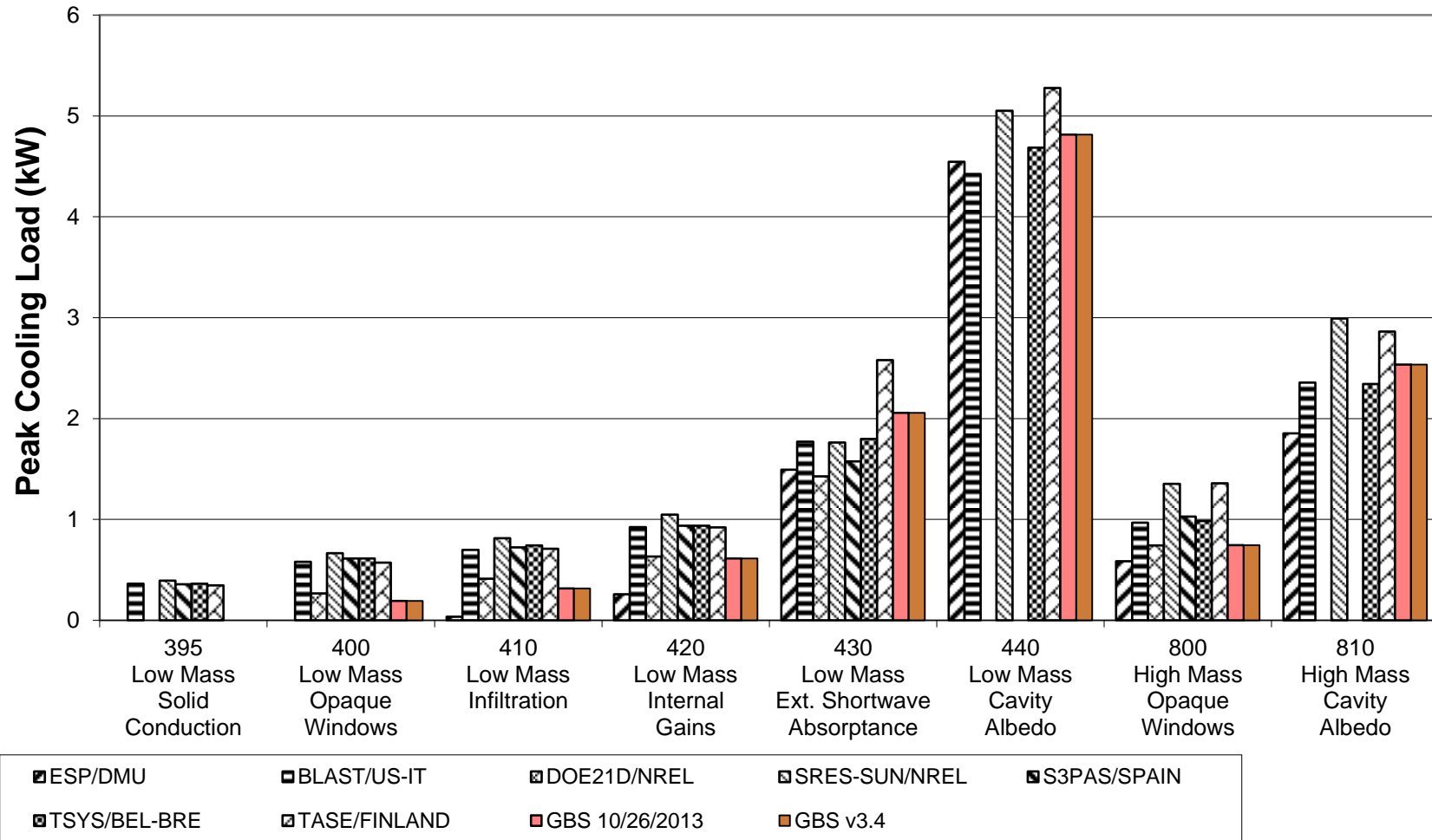
**Figure B8-48. BESTEST IN-DEPTH
 Annual Sensible Cooling
 Cases 395 to 440, 800, 810**



**Figure B8-49. BESTEST IN-DEPTH
 Peak Heating
 Cases 395 to 440, 800, 810**



**Figure B8-50. BESTEST IN-DEPTH
 Peak Sensible Cooling
 Cases 395 to 440, 800, 810**



**Figure B8-53. BESTEST Case 900FF
Annual Hourly Temperature Frequency**

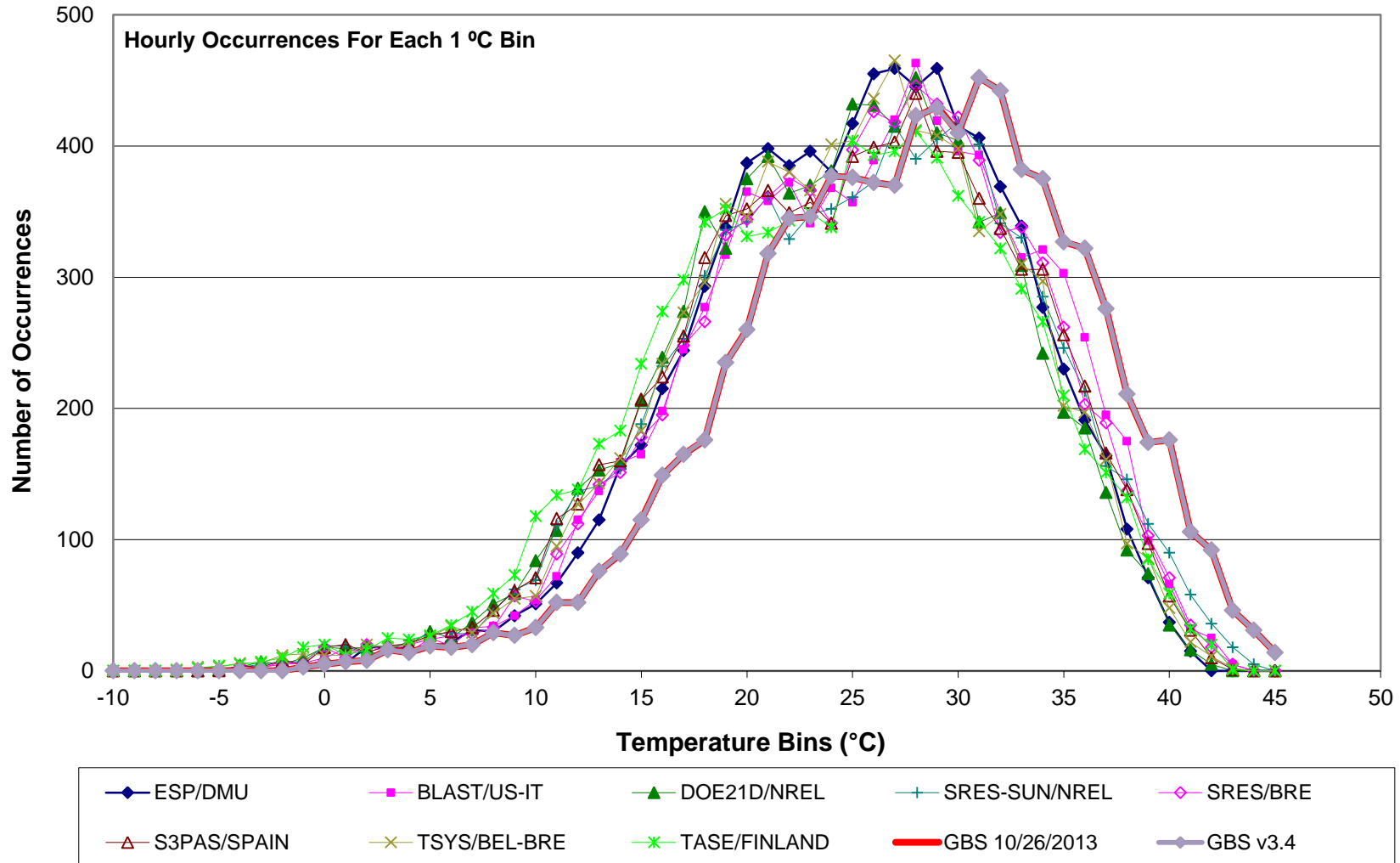


Figure B8-54. BESTEST Case 600
Cloudy & Clear Day Hourly Incident Solar
South Facing Surface

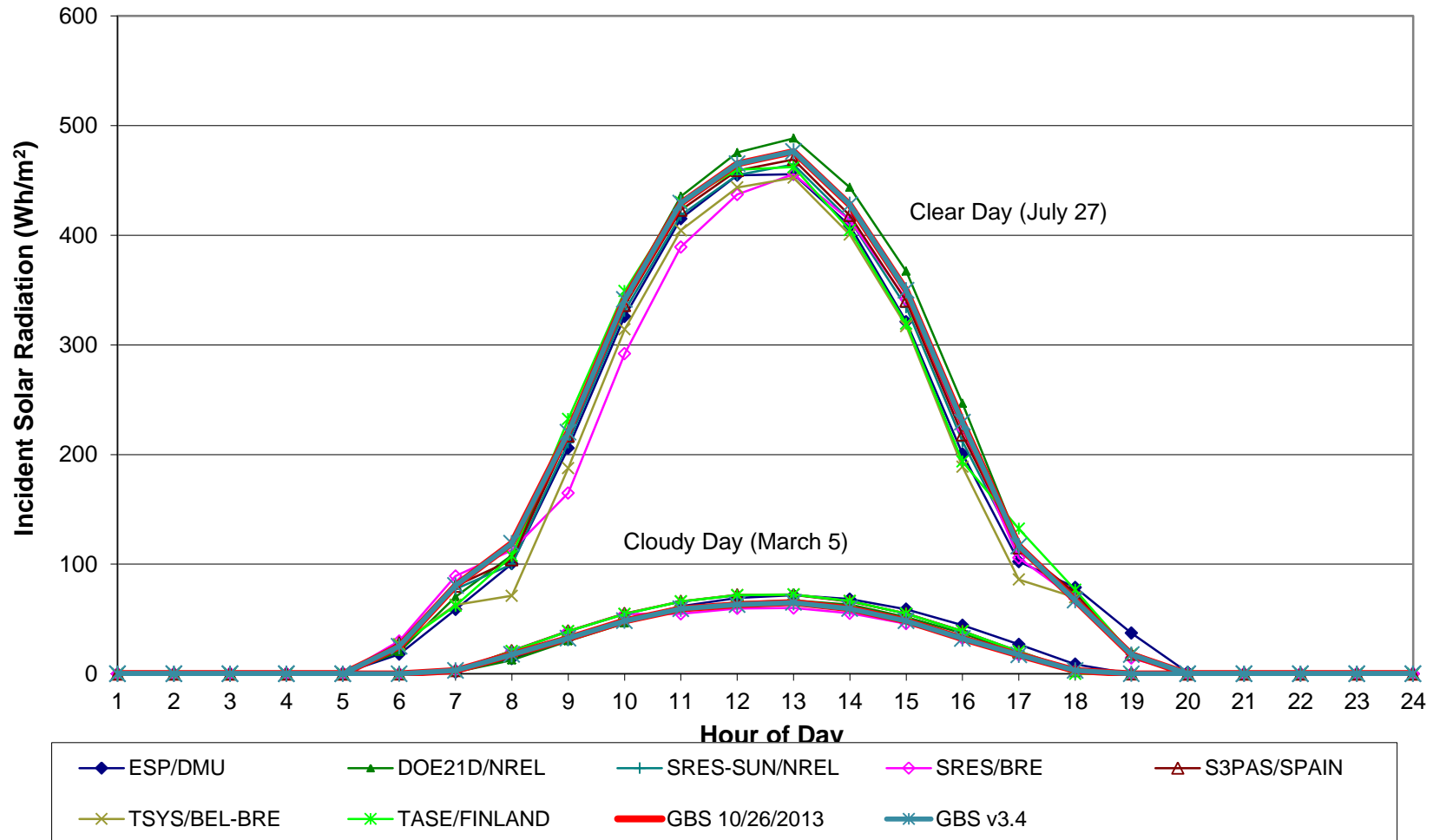
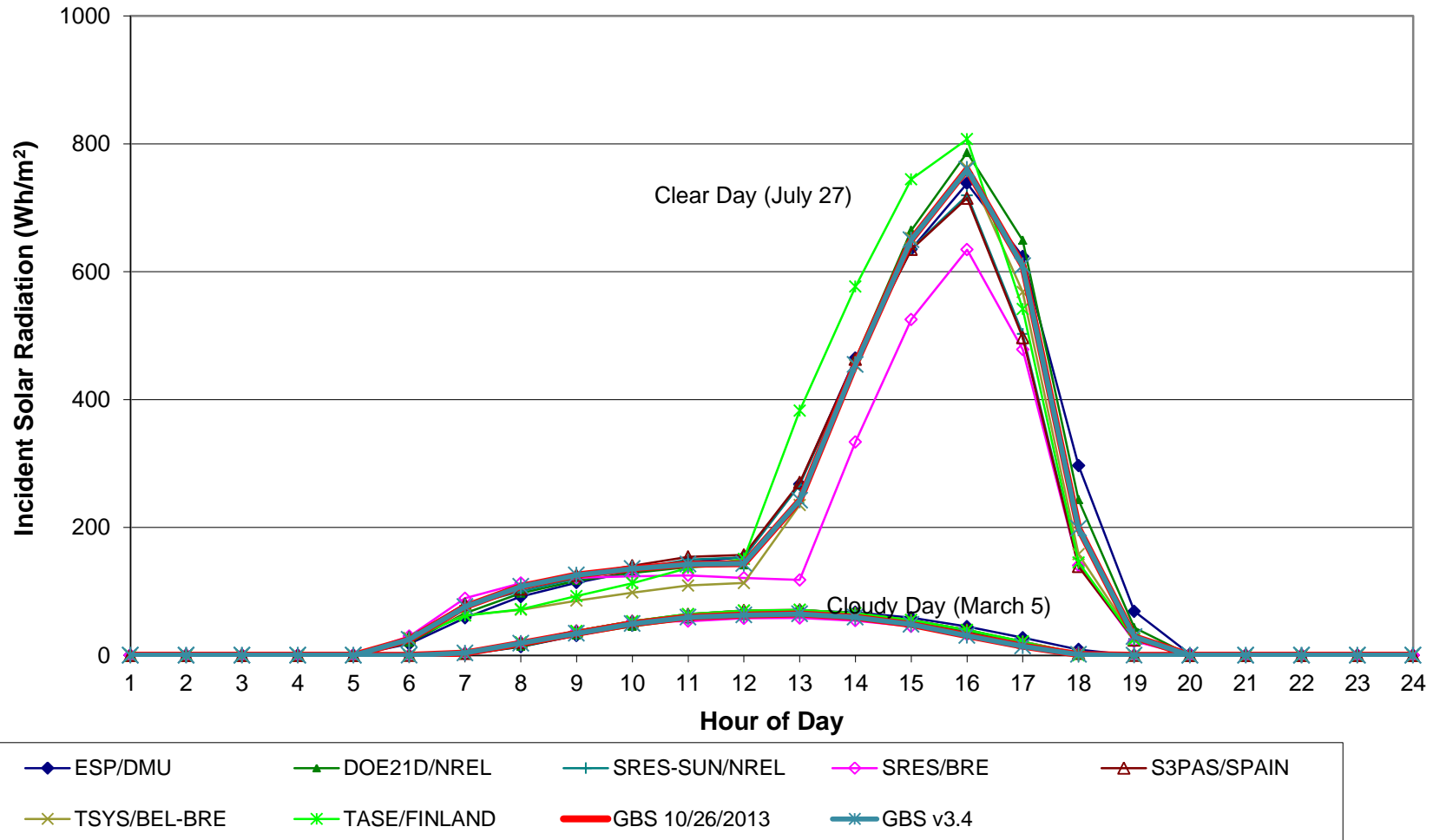
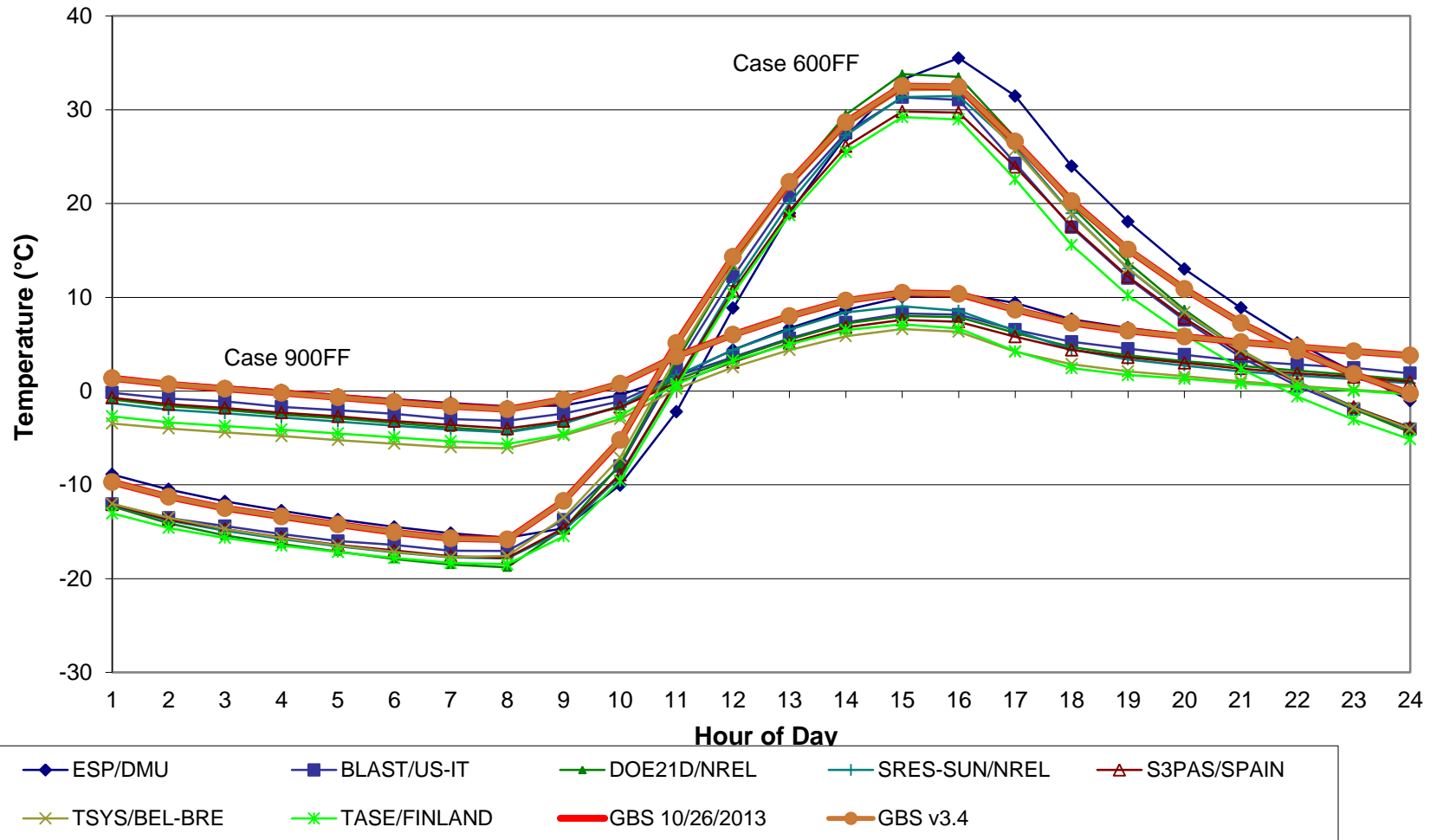


Figure B8-55. BESTEST Case 600
Cloudy & Clear Day Hourly Incident Solar
West Facing Surface



**Figure B8-56. BESTEST
 HOURLY FREE FLOAT TEMPERATURES
 Clear Cold Day - Cases 600FF and 900FF**



**Figure B8-57. BESTEST
HOURLY FREE FLOAT TEMPERATURES
Clear Hot Day - Cases 650FF and 950FF**

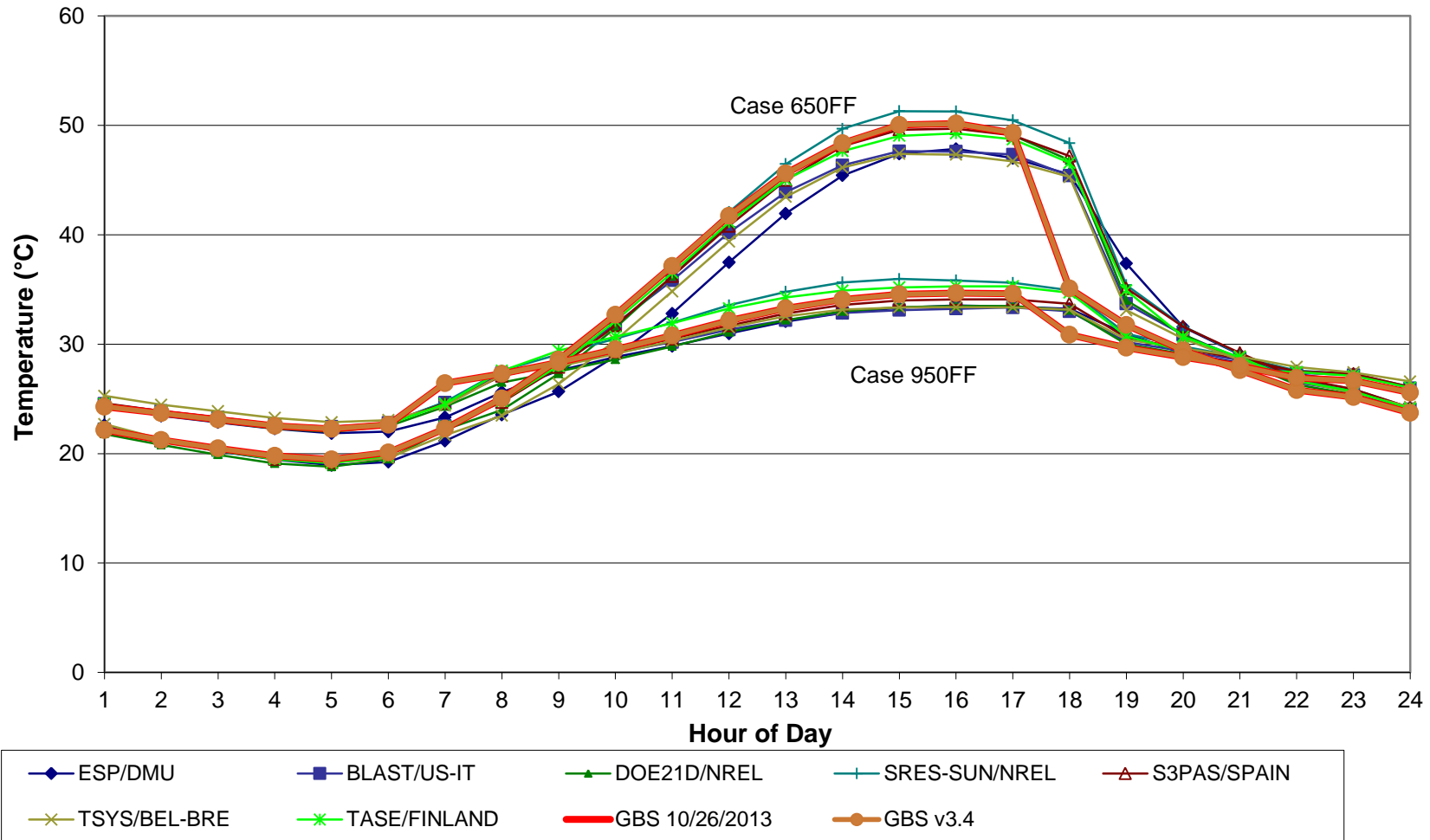


Figure B8-58. BESTEST HOURLY LOADS
Clear Cold Day, Case 600
Heating (+), Sensible Cooling (-)

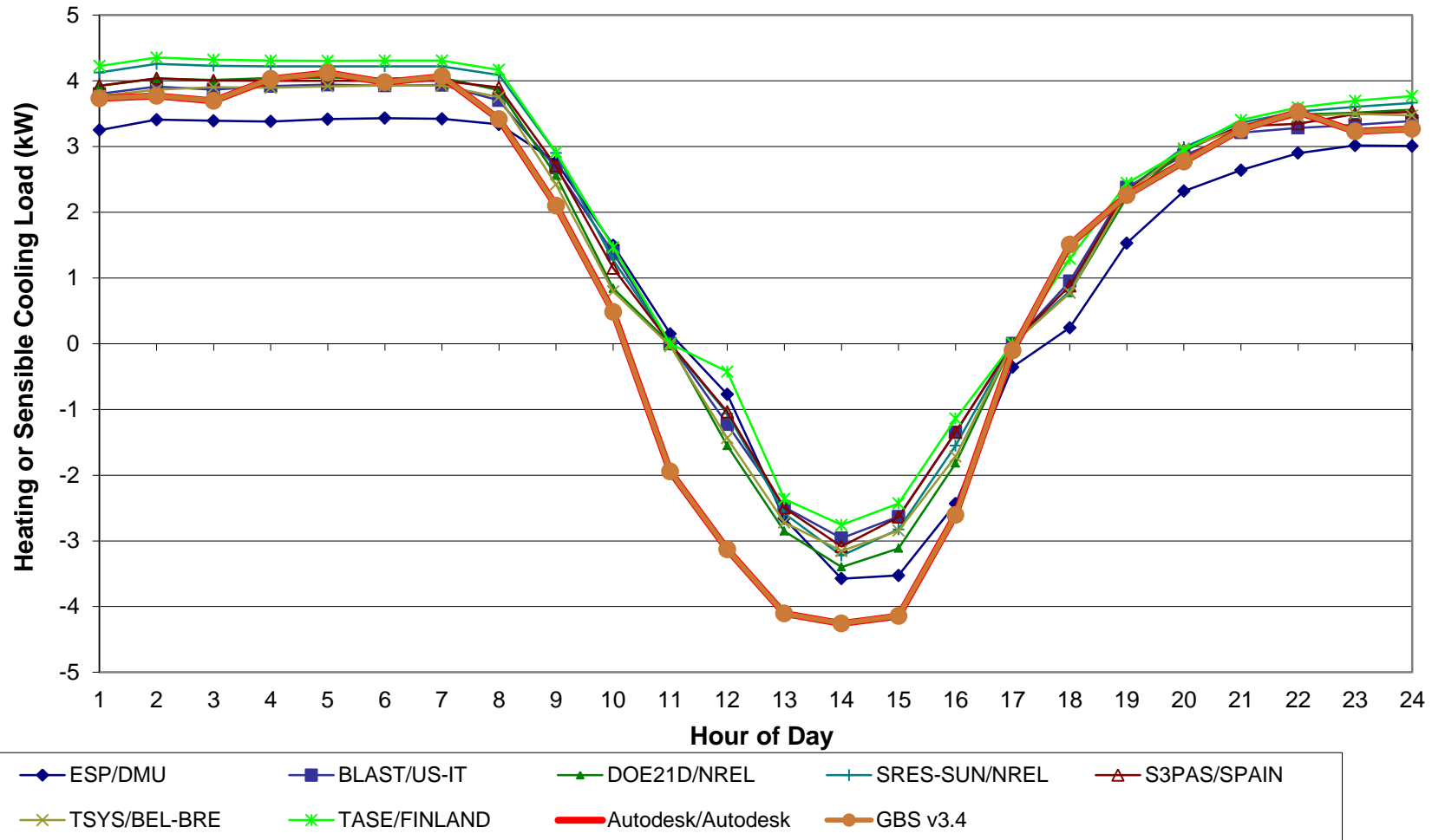


Figure B8-59. BESTEST HOURLY LOADS
Clear Cold Day, Case 900
Heating (+), Sensible Cooling (-)

